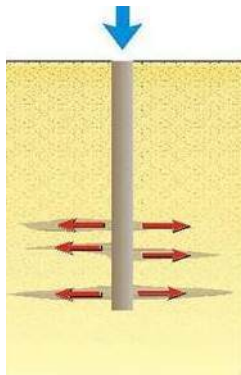


# *Jet Grouting*

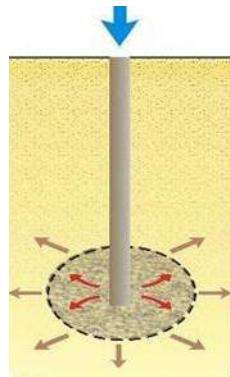


1. Basic principles
2. Main features
3. Required equipment and jobsite organization
4. Quality controls
5. Recent innovations by Trevi
6. Typical applications in Hong Kong (by Claudio Borgatti – GM of *Trevi Construction HK*)

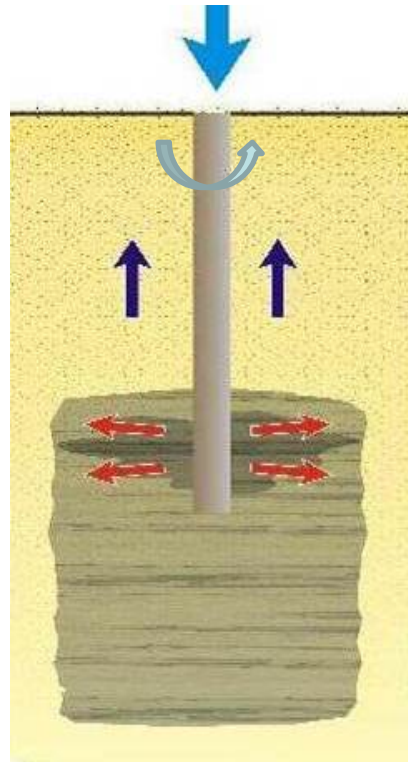
Several methods and relevant technologies are nowadays available for improving hydraulic and mechanical characteristics of soft and loose soils by means of a binding agent (in a dry or fluid form). Jet Grouting belongs to this “family” of methods.



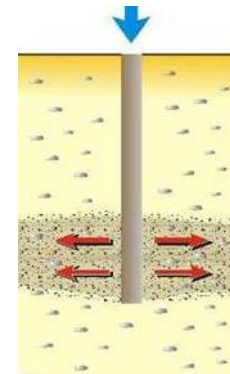
hydraulic  
fracturing



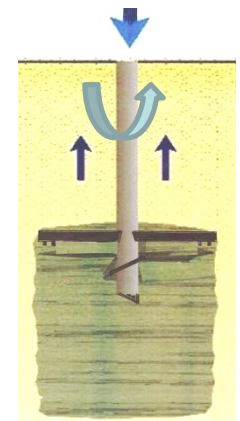
compaction  
grouting



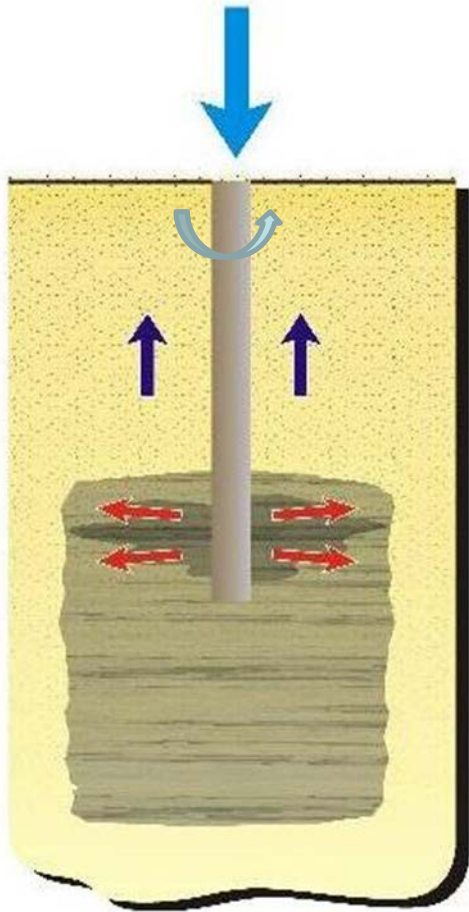
jet grouting



permeation  
grouting



deep soil  
mixing



Jet Grouting is an improvement method that involves the erosion of the in-situ soil structure by means of high energy jets of one or more fluids and its mixing in place with a cement grout mix.

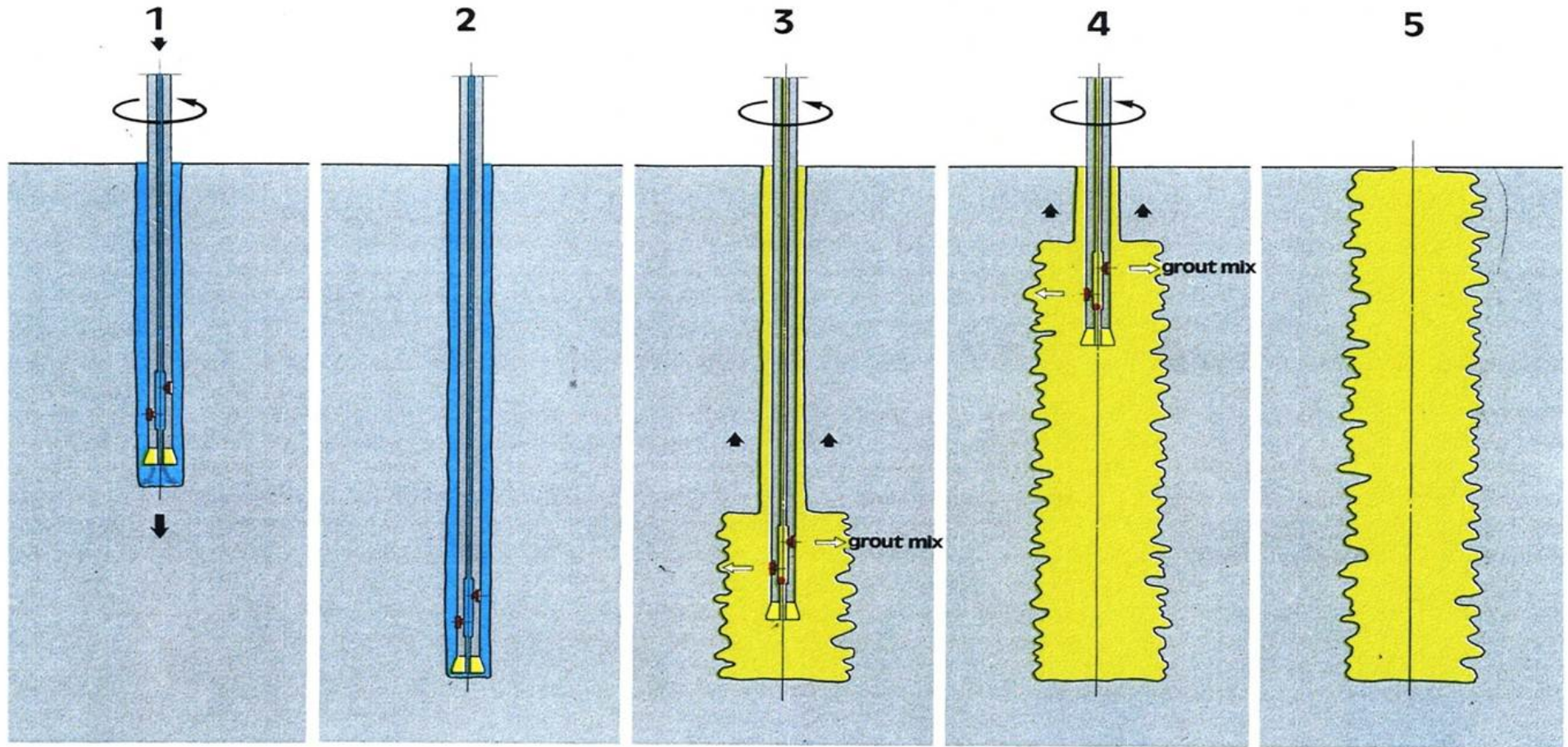
For all members of the European Committee for Standardization (ECS), the applicable standard for the execution, testing and monitoring of JET GROUTING WORKS is:

EN 12716:2001

*"Execution of special geotechnical works – Jet Grouting"*



- 1965/70      conception and first experiments (Yamakado, Japan);
- 1970          development of the "*single-fluid*" system ("*Chemical Churning Pile*" or CCP, Nakanishi, Japan);
- 1972          development of the "*double-fluid*" system ("*Jumbo Jet Special Grout*" or JSG, CCP, Japan);
- 1975          development of the "*triple-fluid*" system ("*Column Jet Grout*" or CJG, Kajima Corporation, Japan);
- 1980/...      successful introduction in Europe and worldwide diffusion mainly through Italian and German specialized contractors



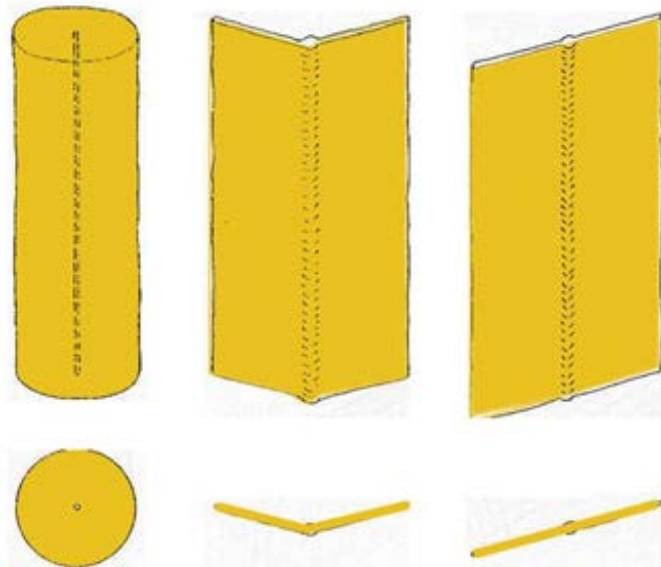
Rotary, roto-  
percussion  
or DTHH drilling

Achieving the  
design depth

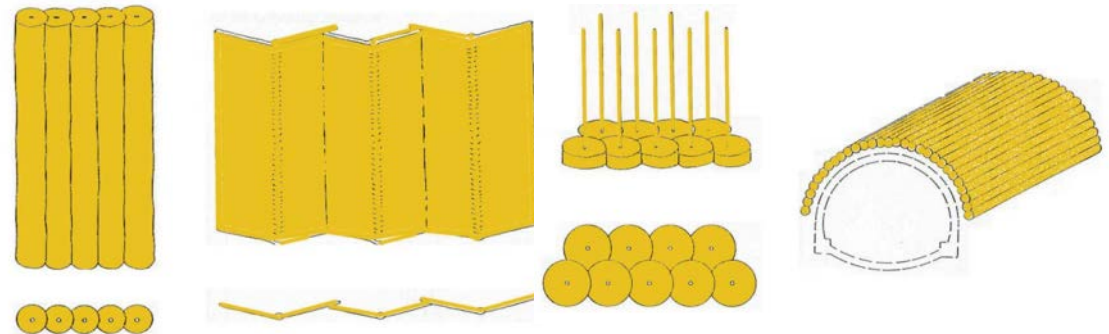
High pressure injection  
while turning and  
extracting the rods in a  
controlled manner

Continue the  
process up to the  
design top  
elevation

Completed  
column of treated  
soil

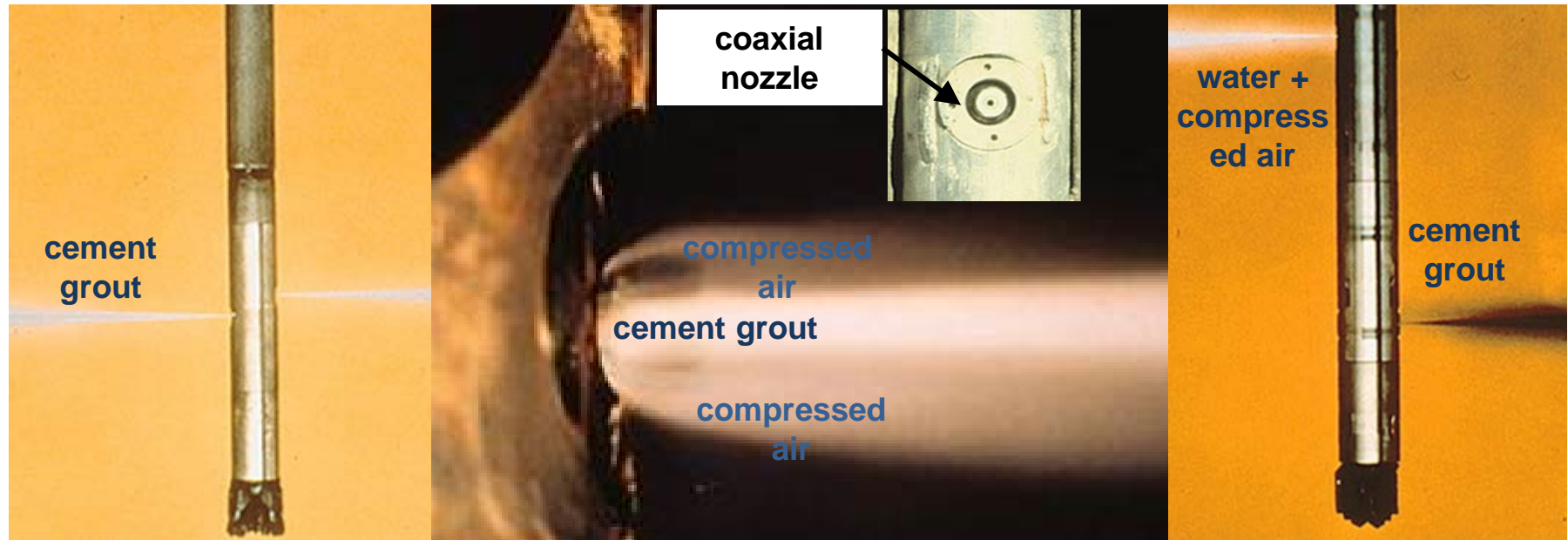


basic elements  
(columns and thin panels)



complex structures  
(by combining basic elements)

The high-velocity jets are achieved by pumping the fluids at high pressure and forcing them to exit from small diameters (2÷6 mm) nozzles located at the bottom of the drilling rods.



## “single-fluid”

one single fluid (cement grout) for both, eroding and cementing the soil

## “double-fluid”

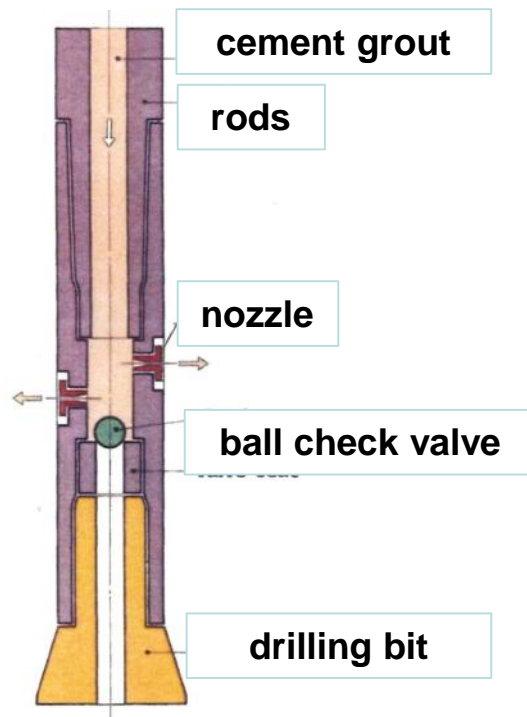
two fluids (cement grout & compressed air) for both, eroding and cementing the soil

## “triple-fluid”

two fluids (water & compressed air) for eroding and one fluid (cement grout) for cementing the soil



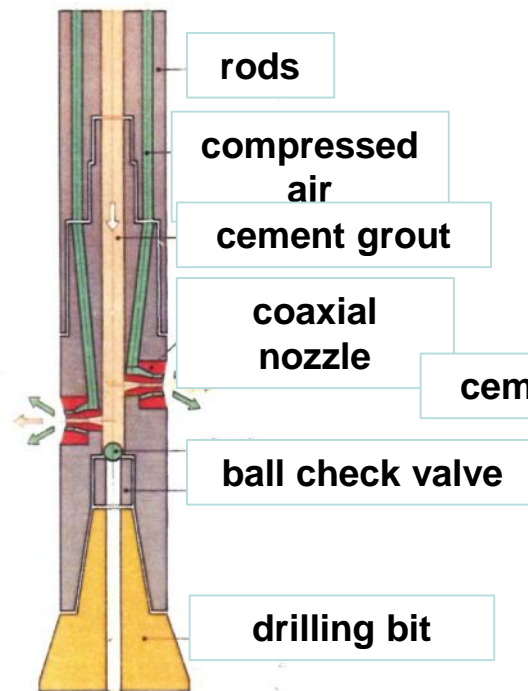
The effect of the compressed air is to increase the radius of action of the grout ("double-fluid") or water ("triple-fluid").



**"single-fluid"**

Typical column's  
diameters:

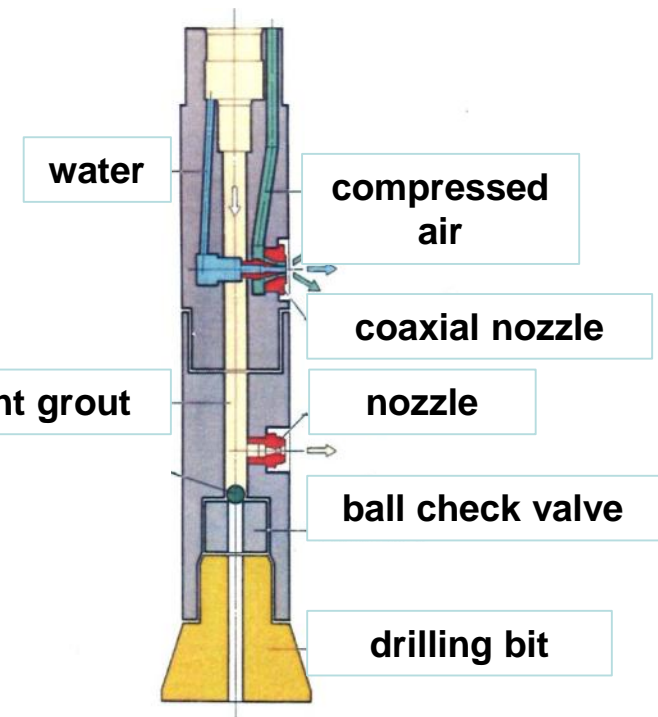
40 ÷ 120 cm



**"double-fluid"**

Typical column's  
diameters:

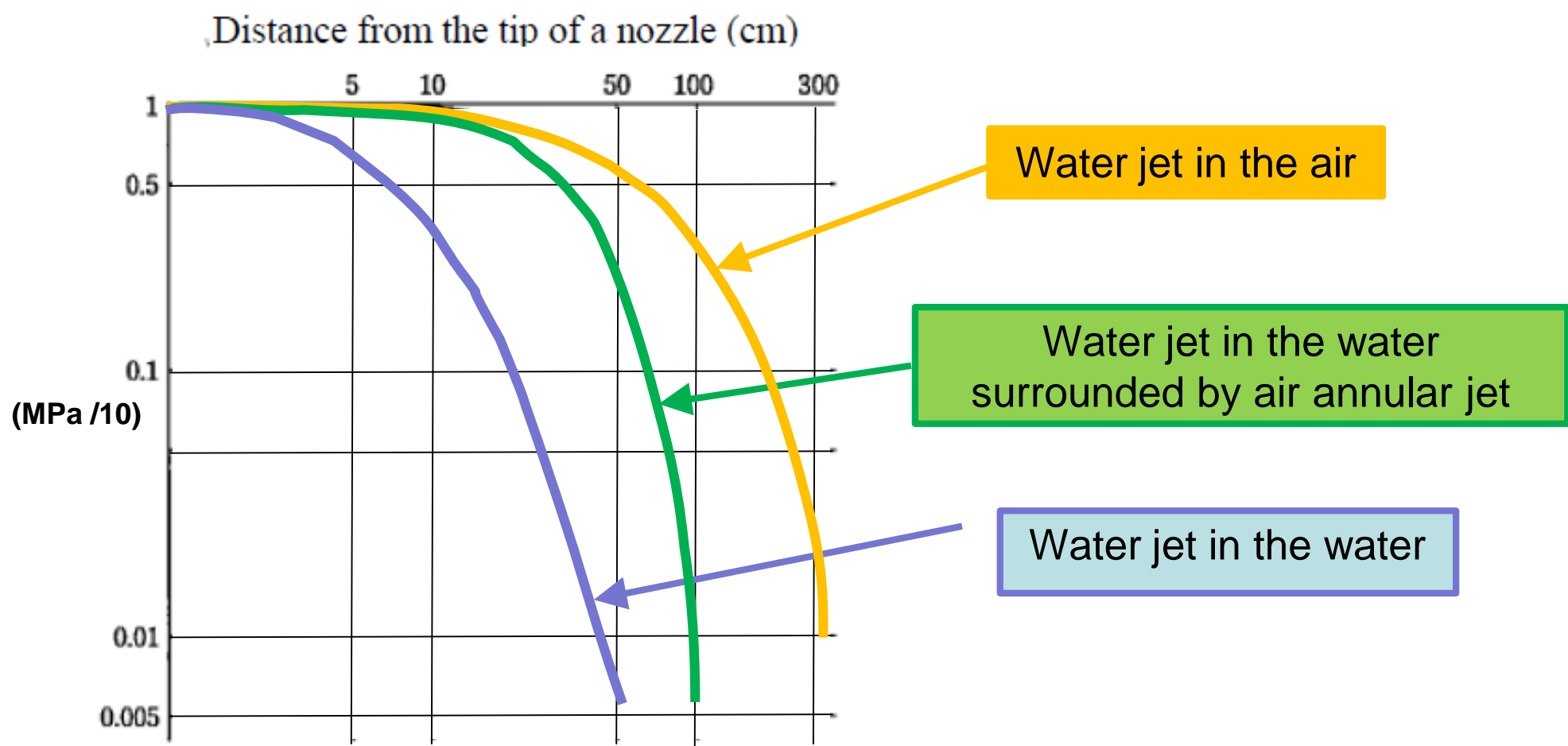
80 ÷ 250 cm



**"triple-fluid"**

Typical column's  
diameters:

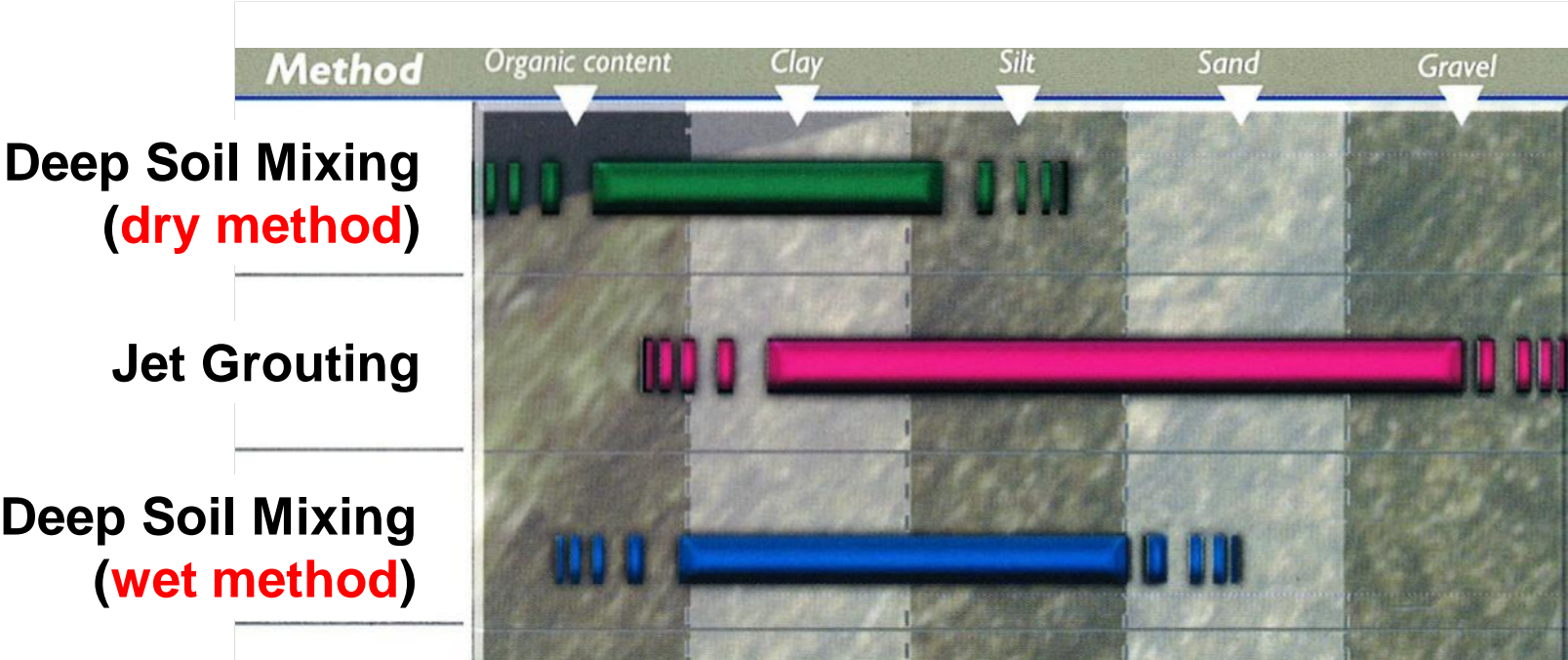
200 ÷ 400 cm



<i>Parameter</i>		<i>"single fluid"</i>	<i>"double fluid"</i>	<i>"triple fluid"</i>
Grout pressure	(MPa)	30÷50	30÷50	6÷20
Grout flow rate	(l/min.)	50÷450	50÷450	50÷200
Water pressure	(MPa)	-	-	30÷50
Water flow rate	(l/min.)	-	-	50÷200
Air pressure	(MPa)	-	0,2÷1,7	0,2÷1,7
Air flow rate	(m <sup>3</sup> /min.)	-	3÷12	3÷12
Rods rotation speed	(r.p.m.)	6÷20	6÷20	6÷20

Final working parameters shall always be selected according to the results of one or more preliminary full-scale trial fields to be performed in the same area(s) of intervention.

Among all other soil improvement methods involving the use of a binding agent, Jet Grouting is the one applicable to the largest range of soils.







The achievable diameters depend on a large number of factors, the main of which is the erodibility of the concerned soil.

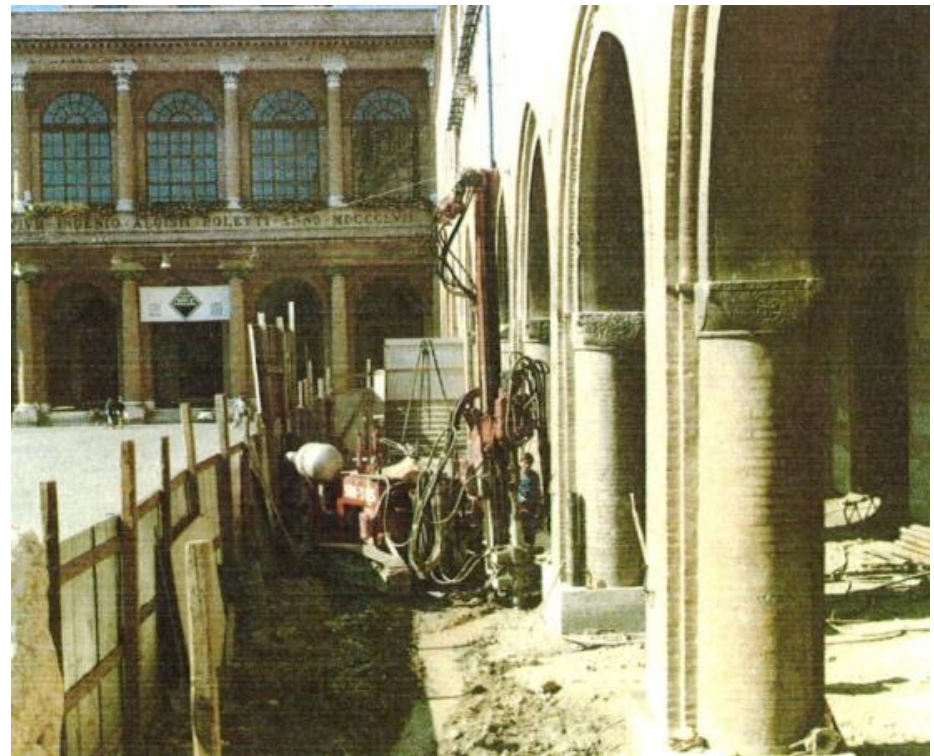
Loose coarse gravel



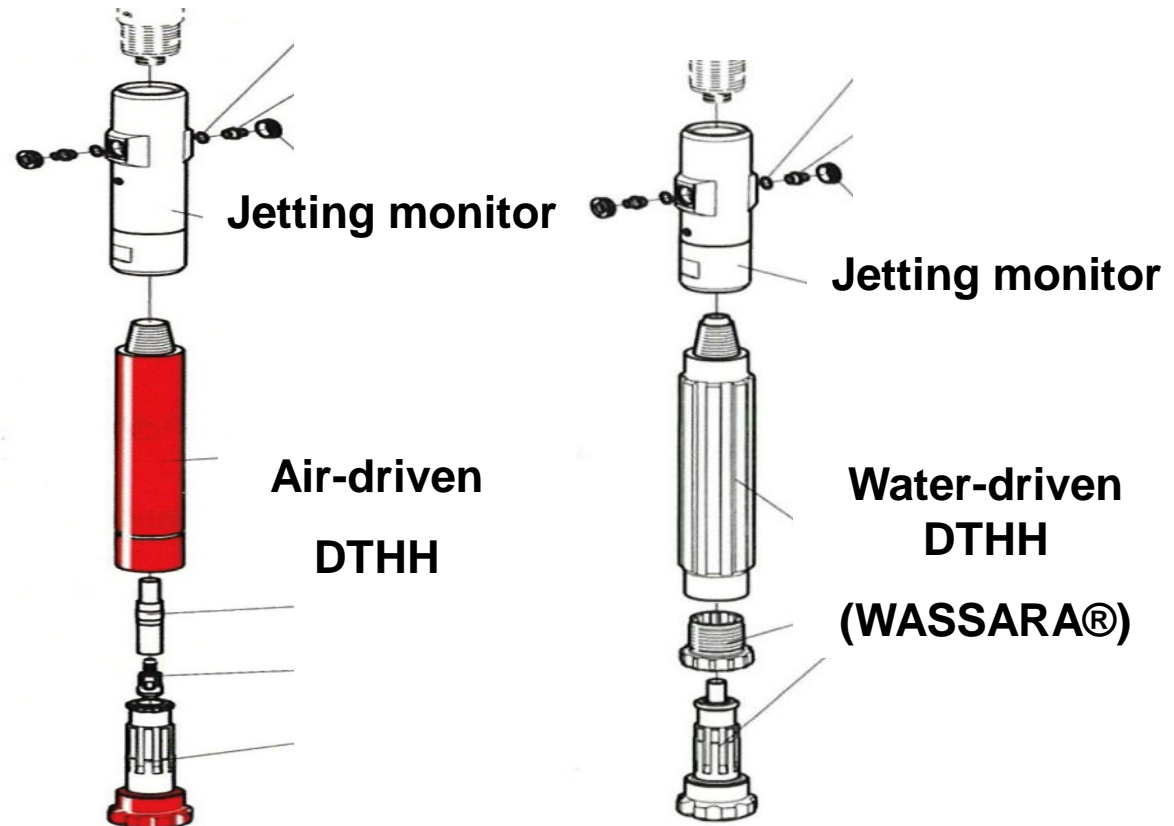
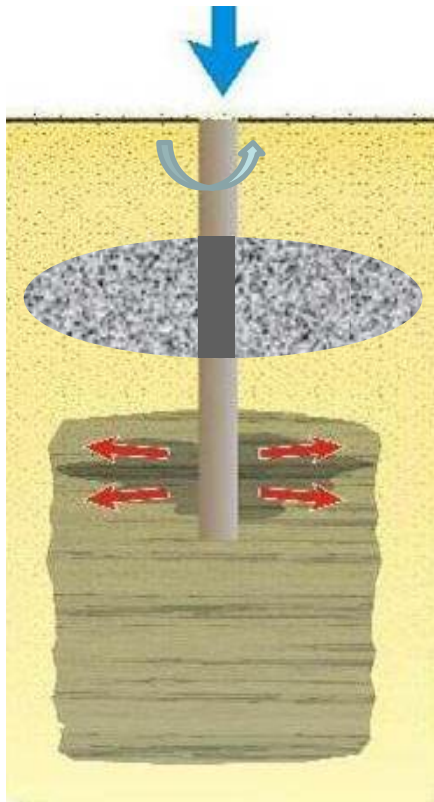
Plastic clay



Starting from a small diameter drilled hole ( $100 \div 180$  mm), it is possible to produce a consolidated soil column up to 4 m in diameter. As a result of this, also small drilling rigs can be employed for performing Jet Grouting and small working spaces do not hamper its employment.



By using the most appropriate drilling technology, it is possible to pass through natural (i.e. boulders, rocky formations etc.) or man-made (i.e. old masonry or concrete foundations etc.) obstacles.





## “single-fluid”



Hydraulic drilling rig with  
automatic  
grouting parameters recorder



Automatic high capacity  
(20-25 m<sup>3</sup>/h) grout batching plant



High pressure (40-60 MPa)  
grout pump

## “double-fluid”

+



High capacity  
(20 m<sup>3</sup>/min at 2 MPa)  
air compressor

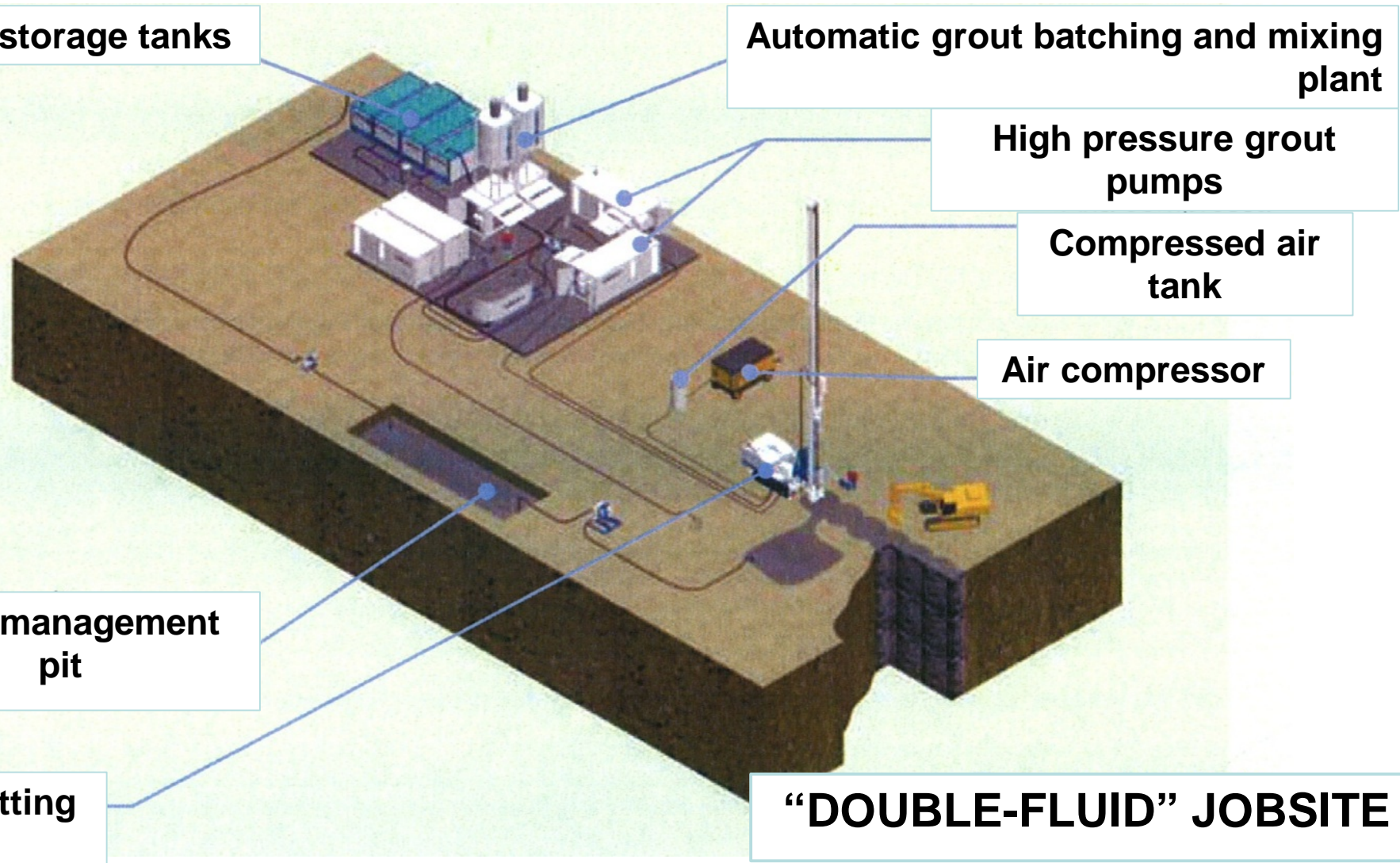
+



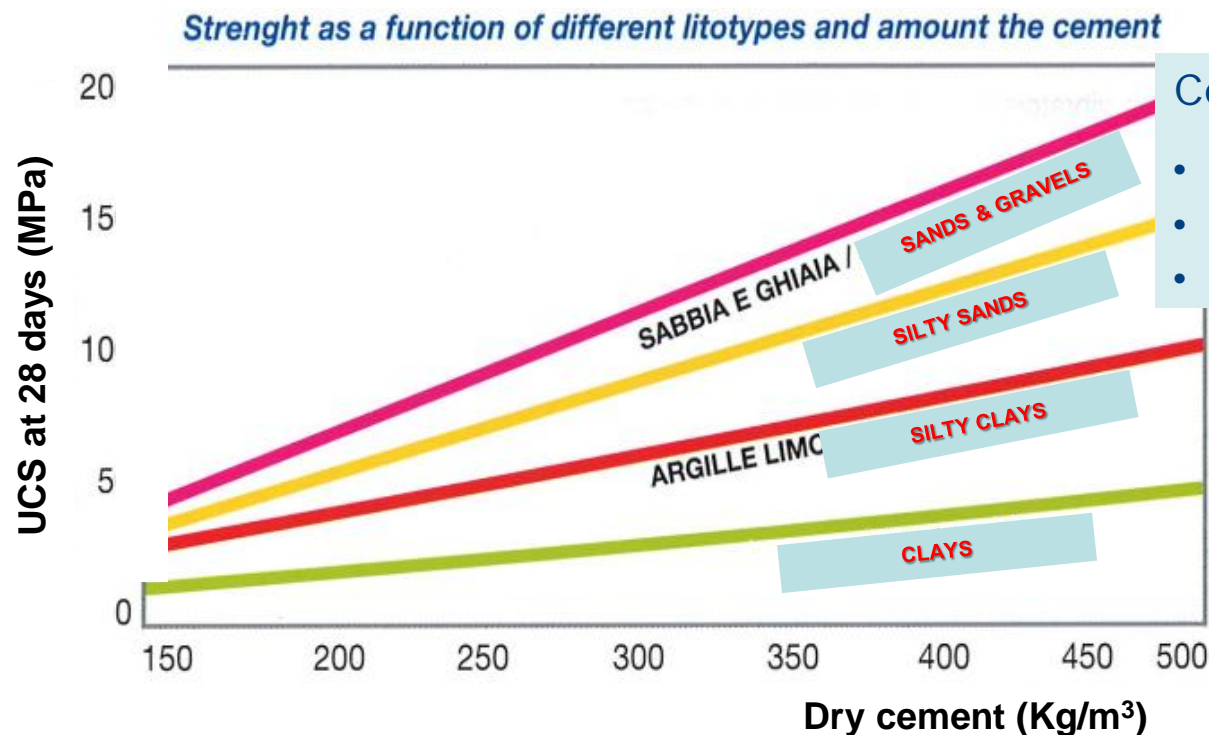
Medium pressure  
(20-30 MPa)  
grout pump

## “triple fluid”





The final result of the Jet Grouting process is a mix of water, cement and original soil. Consequently, the final strength of the treated soil is directly correlated to two main factors: (1) the nature of the original soil and (2) the quantity of cement introduced into the process.



Cement content (typical quantities):

- single-fluid : 200÷400 kg/m<sup>3</sup>
- double.-fluid : 200÷800 kg/m<sup>3</sup>
- triple-fluid : 400÷1000 kg/m<sup>3</sup>

Concerning permeability, the values usually range between  $10^{-4}$  cm/s and  $10^{-5}$  cm/s, with lower values related to clayey soils.

## Before execution

- Comprehensive soil investigation and testing
- Full-scale trial field(s)

## During execution

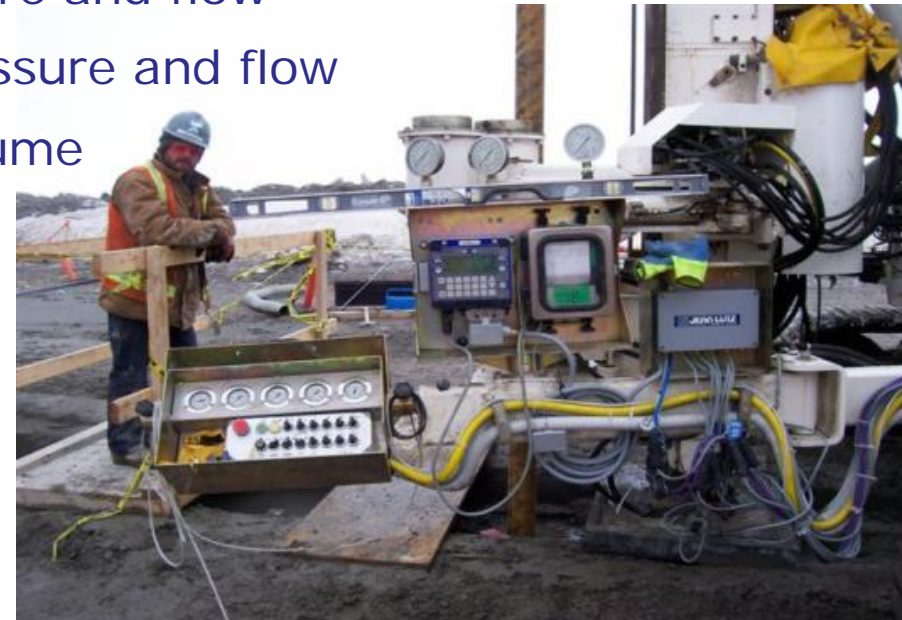
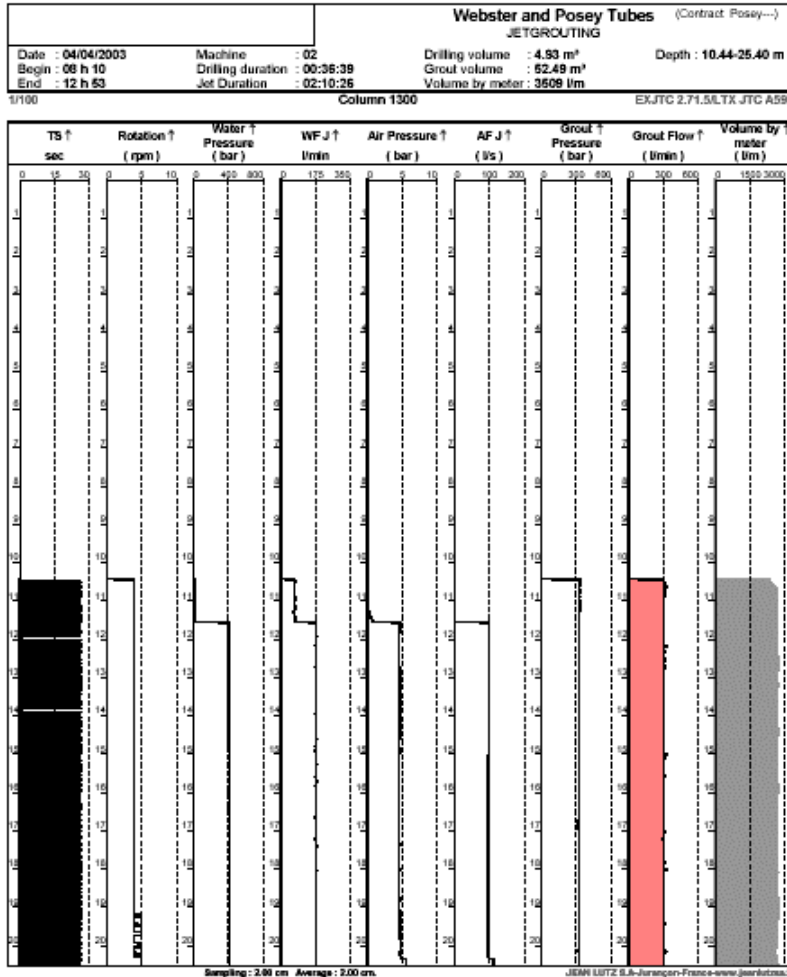
- Rheological characteristics of the grout
- Borehole starting position
- Drilling and jetting parameters
- Borehole deviation
- Free flow of the return spoil

## After execution

- Cored holes
- In-situ testing inside the cored holes
- Laboratory testing on cored samples
- Pumping tests
- Other tests according to the final scope of the intervention

## Jetting Parameters

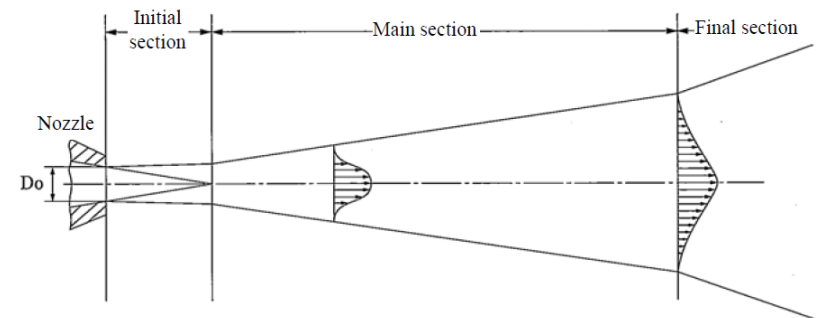
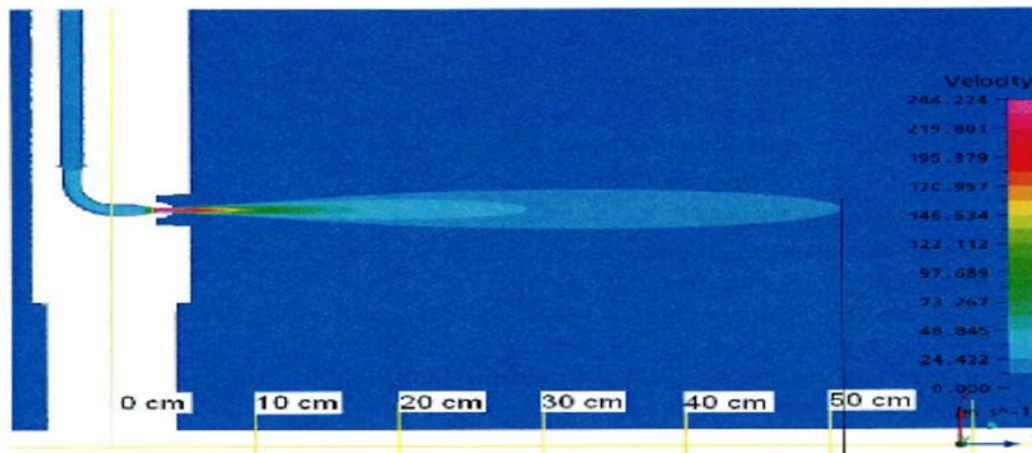
- Depth
- Withdrawal rate
- Rotation speed
- Water pressure and flow
- Air pressure and flow
- Grout pressure and flow
- Grout volume



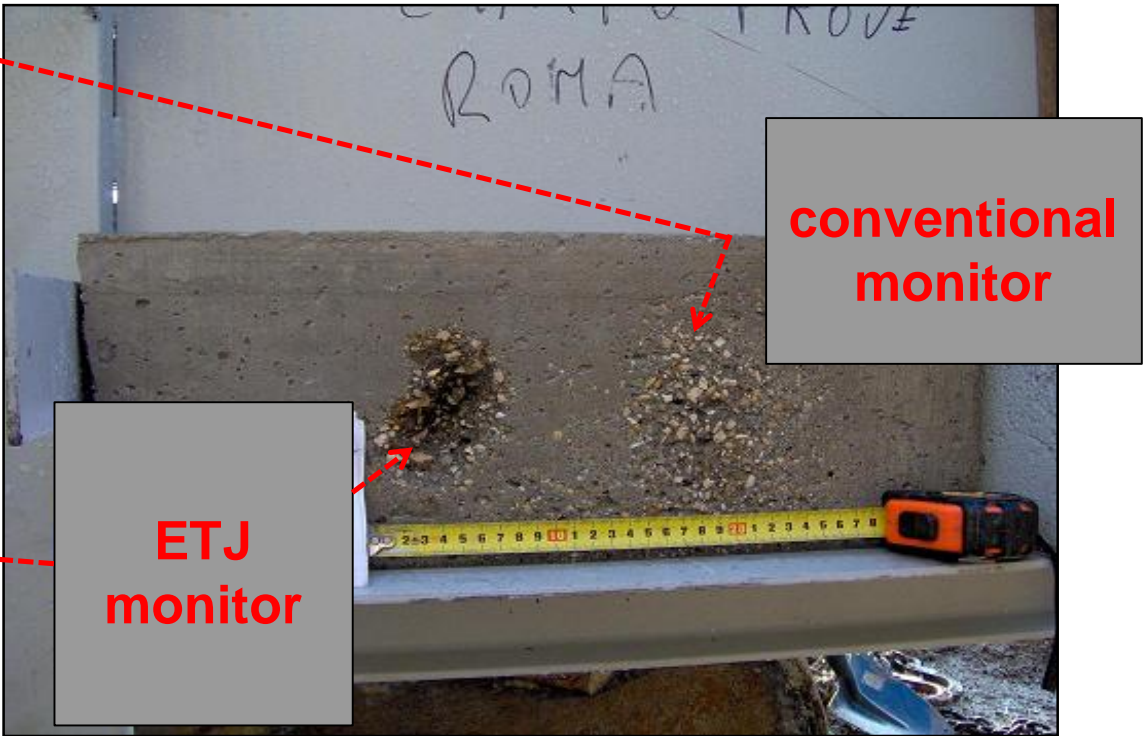


The capability to erode and break up the soil depends on the shape of the jet after its exit from the nozzle. The less the jet widens the greater is its efficiency, and the diameter of the column that can be achieved.

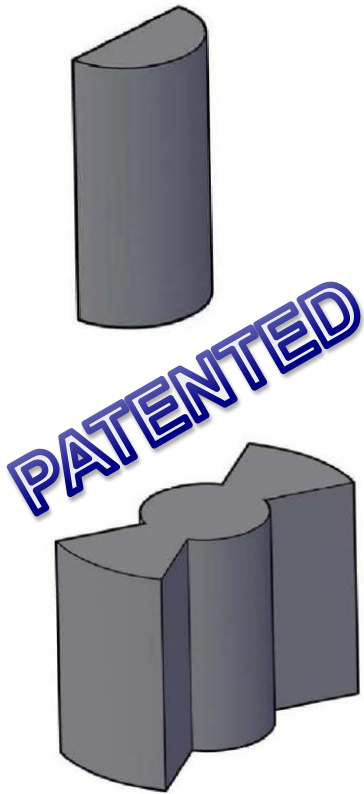
TREVI has carried out extensive theoretical and practical researches on this issue, which has led to the development of a newly-conceived jetting monitor, the Enhanced Trevi Jet (ETJ). In the ETJ, unlike traditional monitors, the grout or water flow is “accompanied” in its exit from the nozzle by means of a curved conduit. The result is a much more “close” jet at greater distance.



The ETJ monitor, already applied in dozens of jobsites, proved to be around 20% more efficient than any other conventional monitor, regardless of the nature of the treated soil.

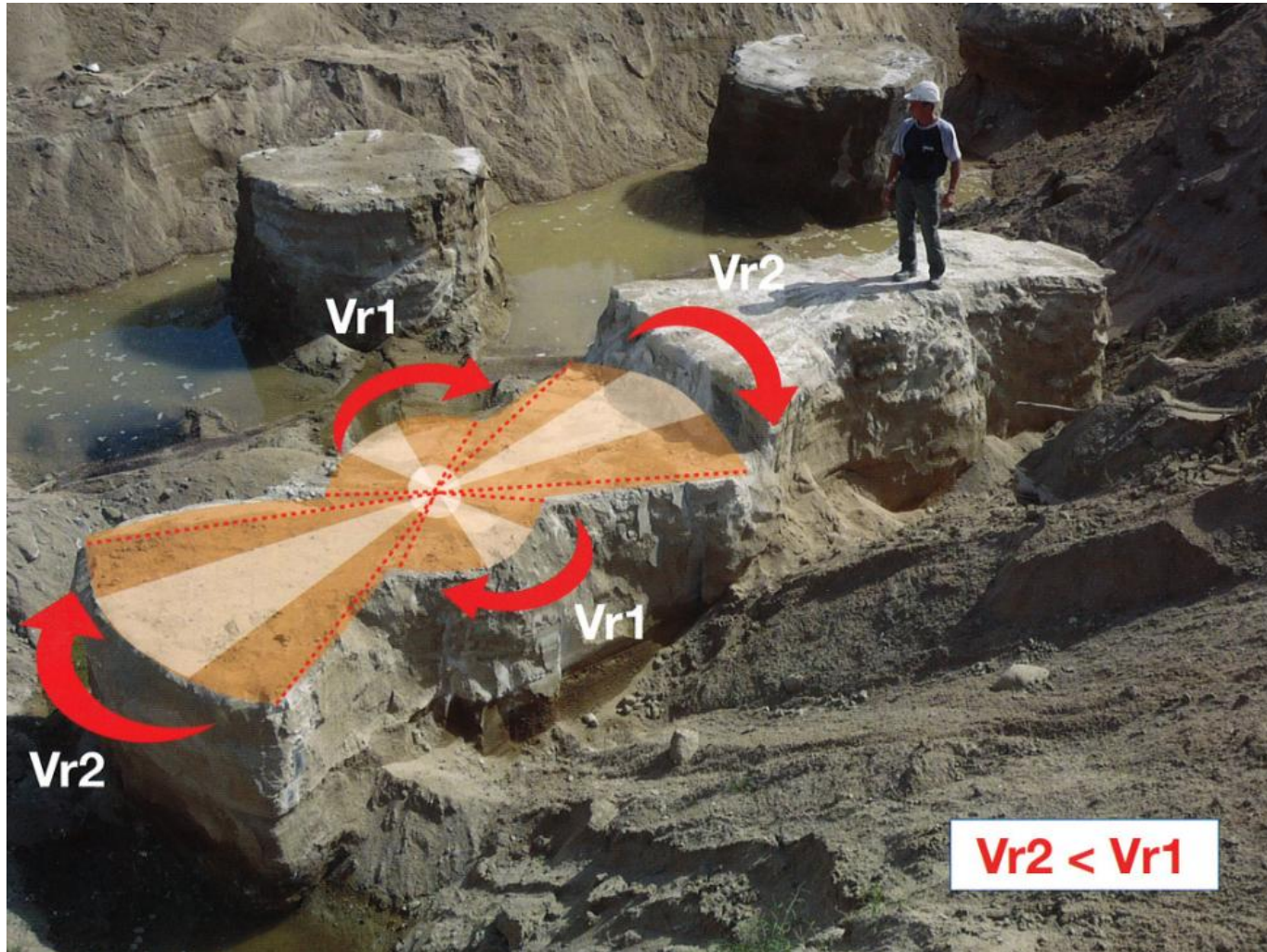


There are some situations where the circular shape of the treated soil is not the most efficient. TREVI has developed and patented a system for performing also different configurations.



$$Vr2 < Vr1$$

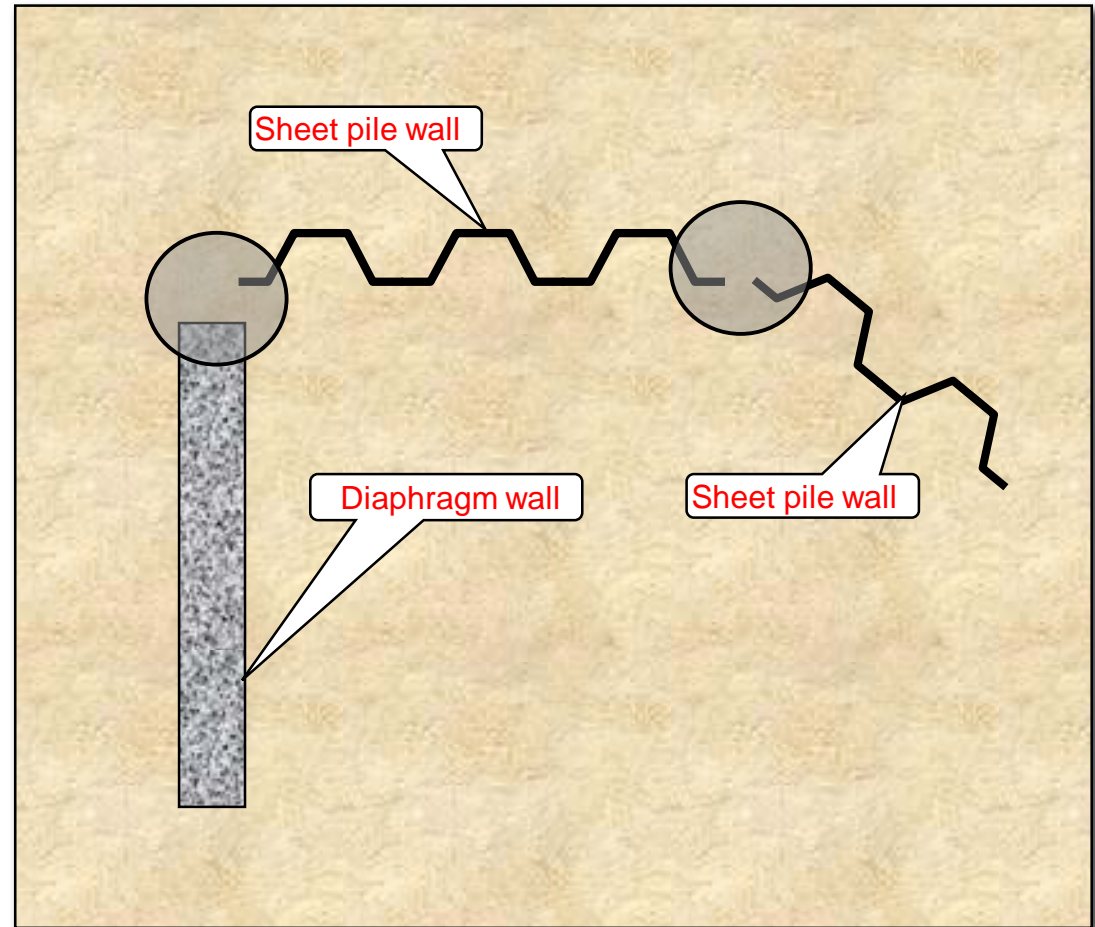






# ***JET GROUTING APPLICATIONS IN HONG KONG***

Closing gaps between adjacent structures (sealing column)



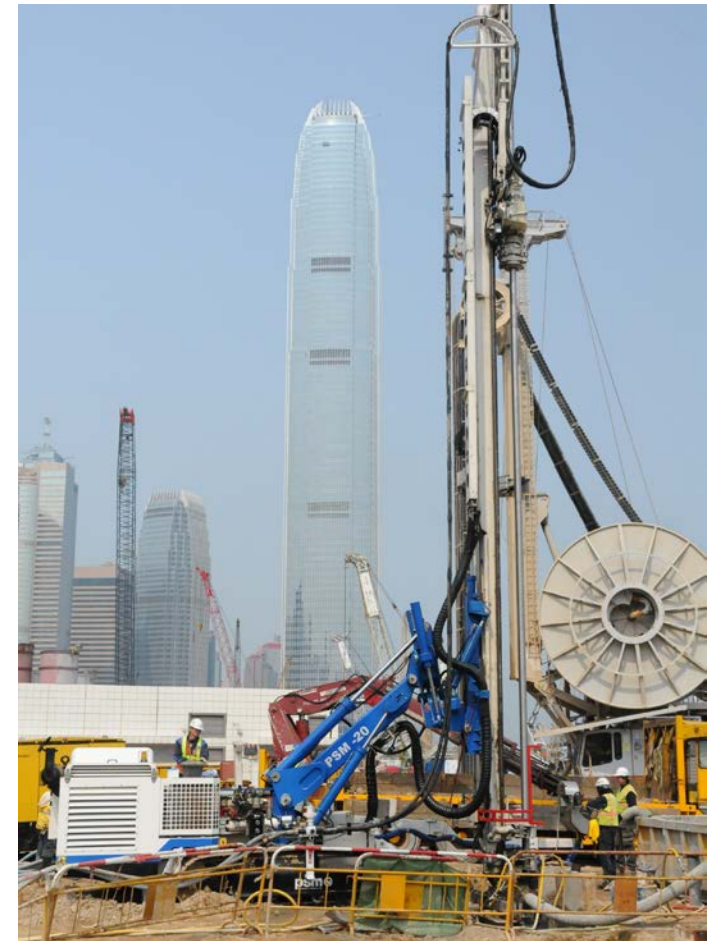
***Project:*** Central Reclamation Phase 3

***Consultant:*** Atkins

***Main Contractor:*** LCSVO JV

***Scope of Works:*** Jet Grouting as cut-off curtain under existing 4-cell culvert for future excavation of Wan Chai by-pass

***Progress :*** Job started in October 2009 and was completed in May 2010

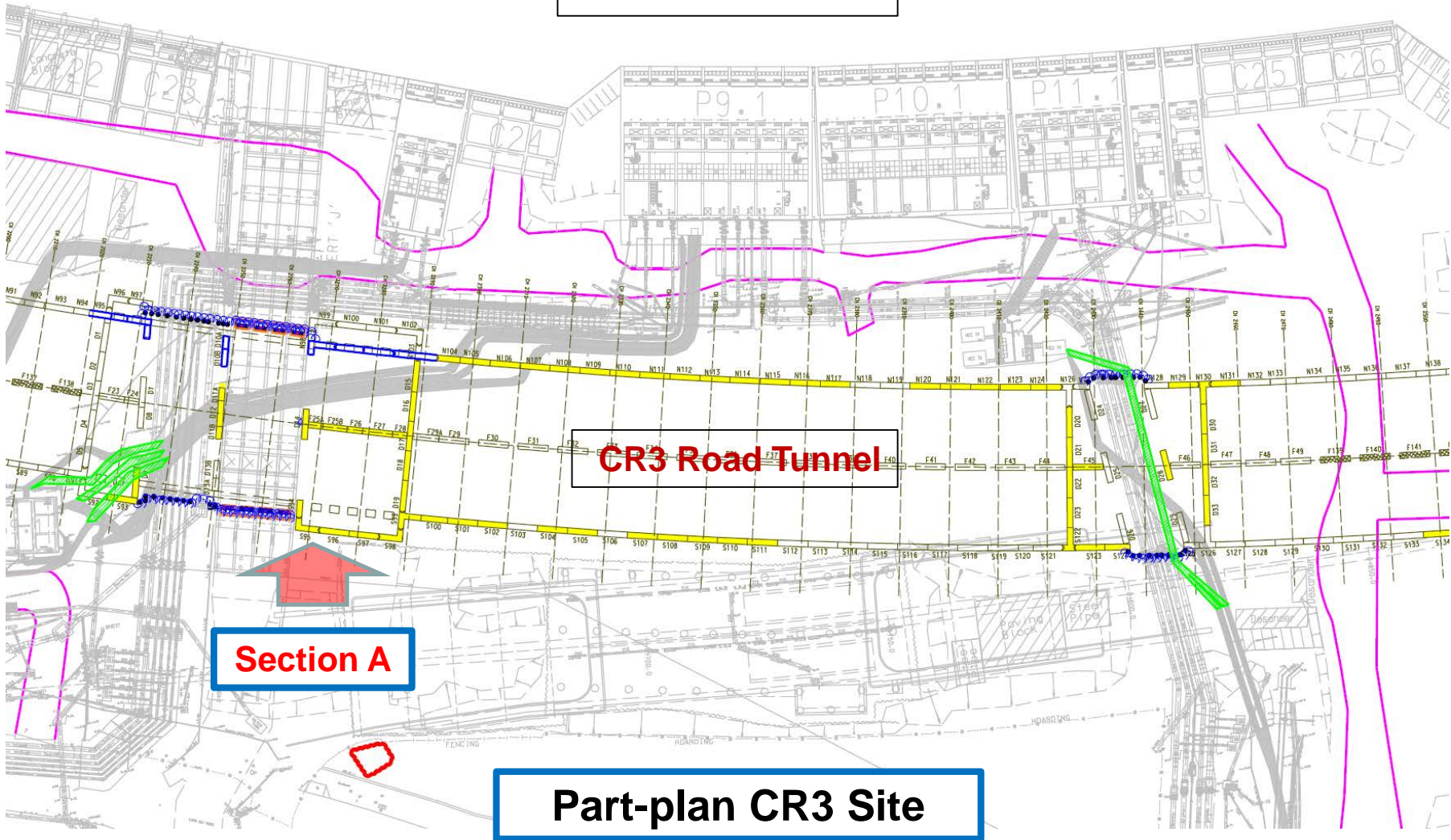


## **Introduction**

- When the CWB road tunnel had been instructed, the 4-cell box culvert and cooling mains crossing the top of the road tunnel in the original Contract had been constructed and installed.
- Driving of continuous D-wall or piles for the cut and cover construction will be difficult.
- Discontinuous pre-bored H-piles and continuous 2.1 m dia. jet grouting columns were installed to support the cut and cover construction and provide the water cut-off required.



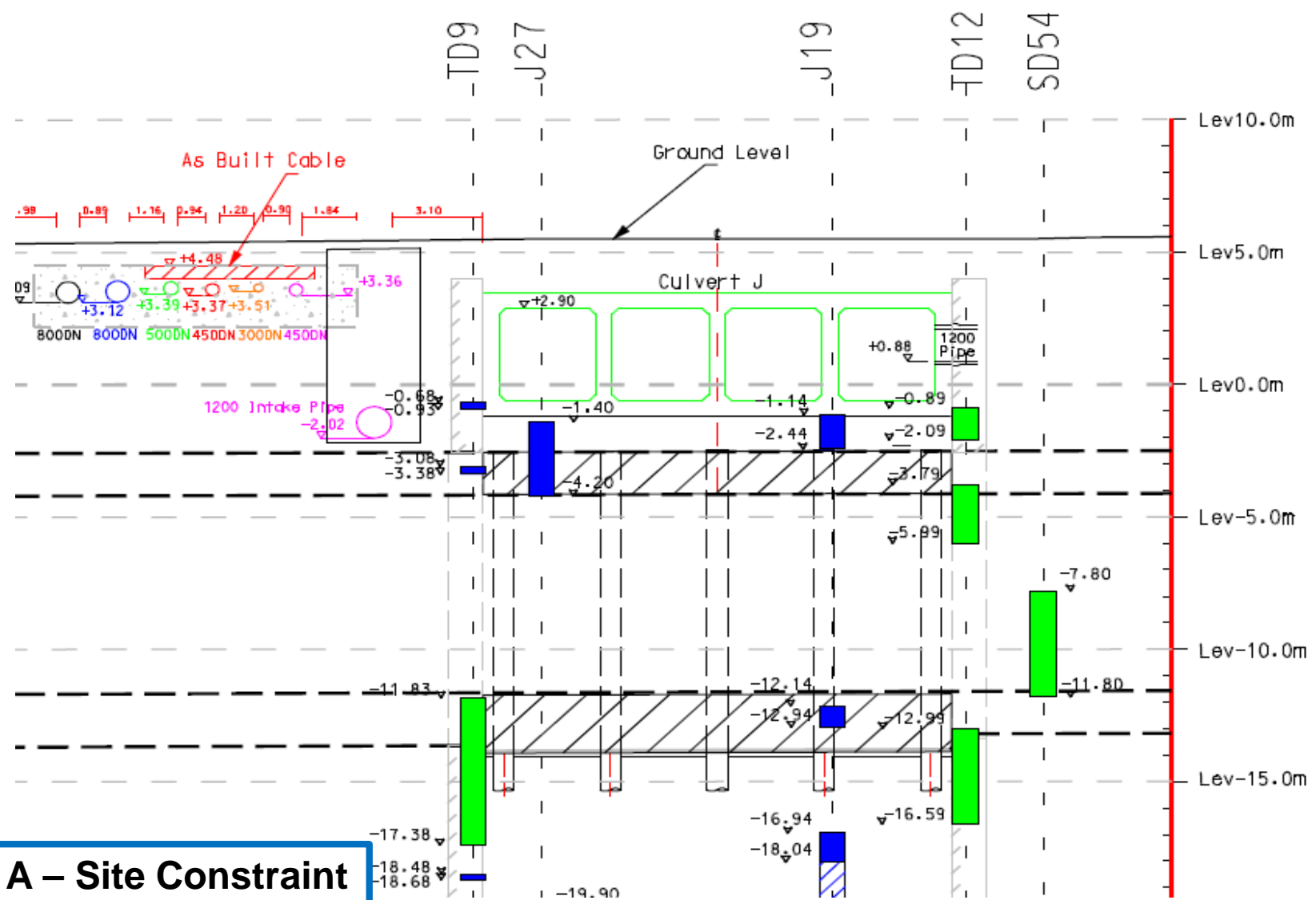
Victoria Harbour



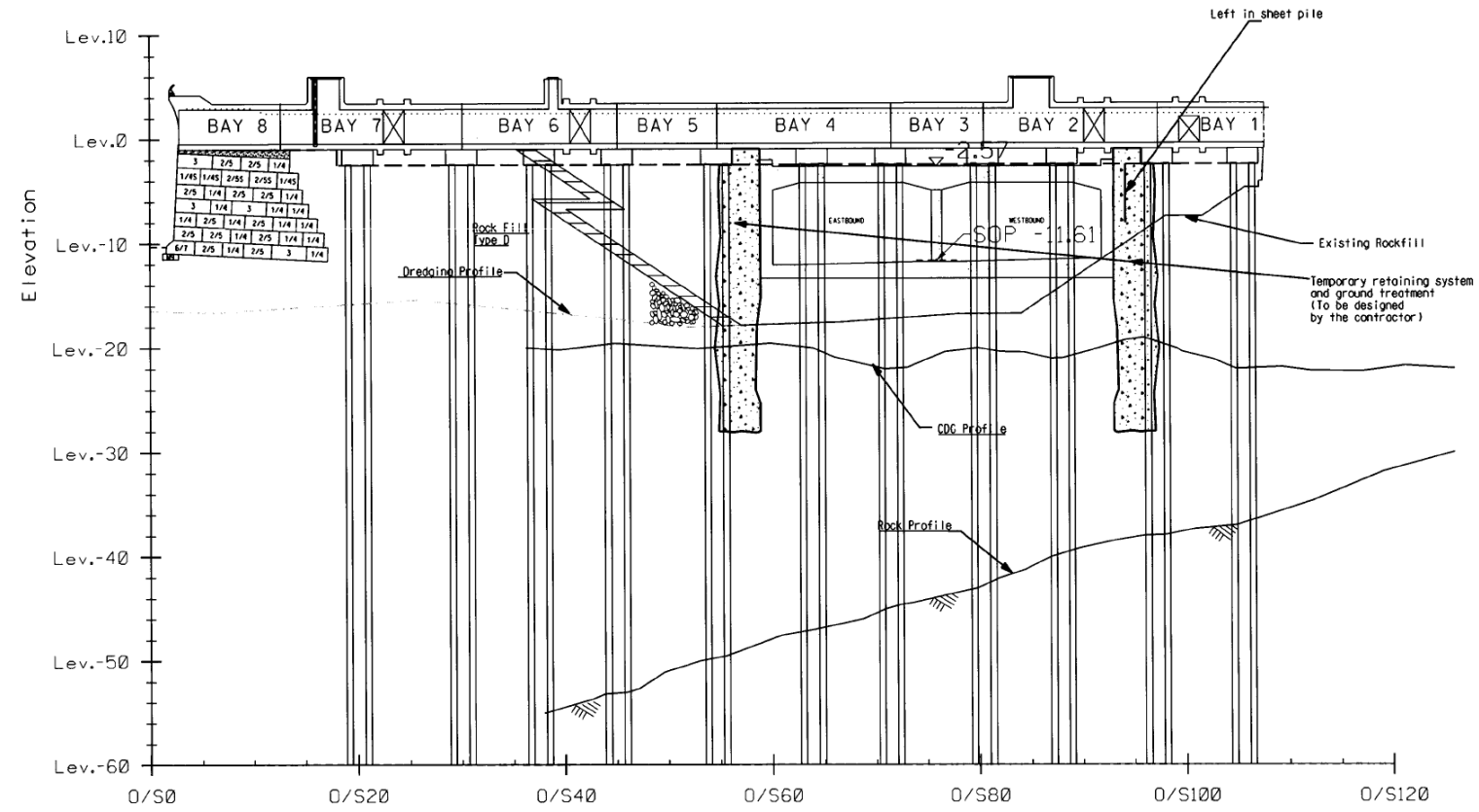
CR3 Road Tunnel

Section A

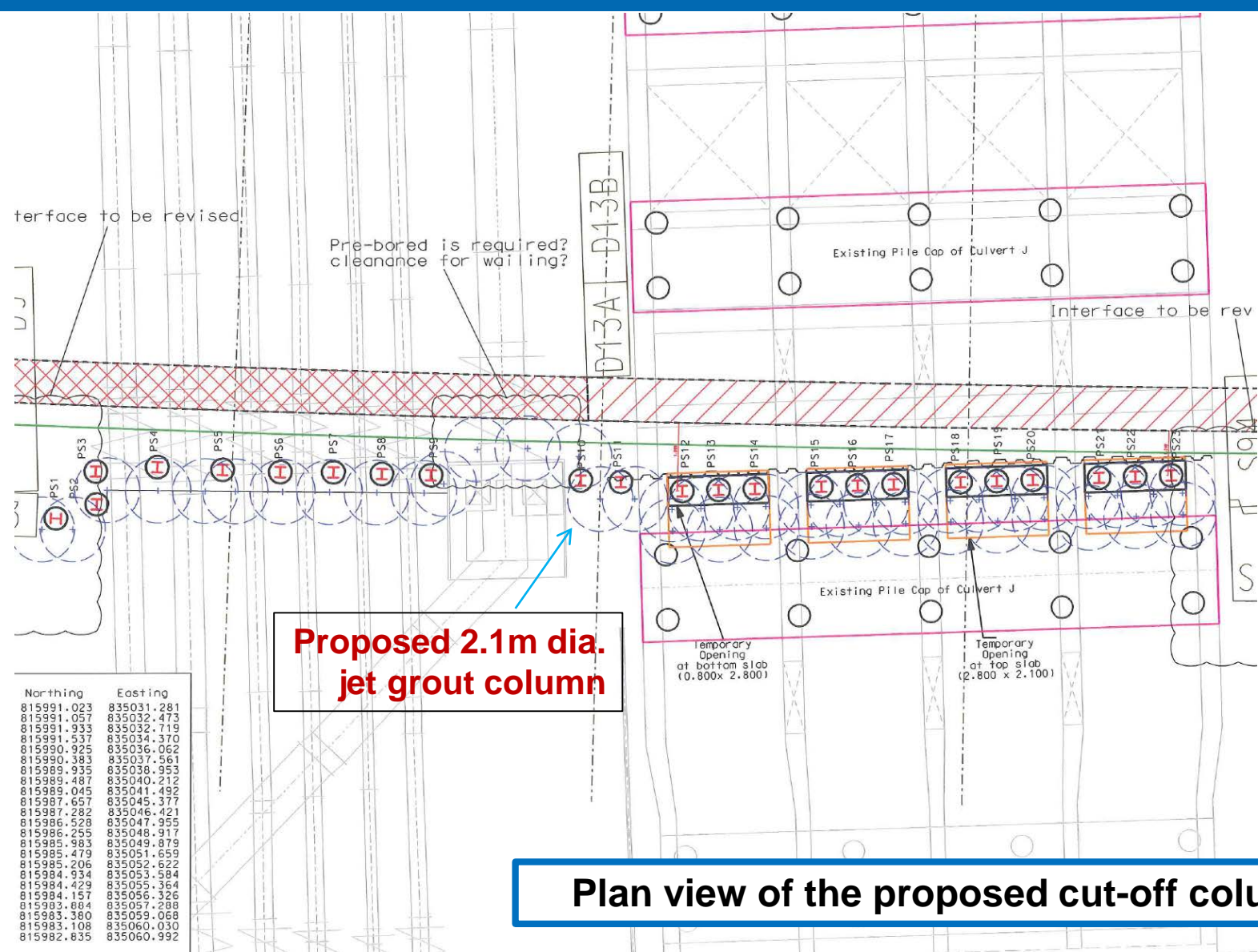
Part-plan CR3 Site



Section A – Site Constraint



Proposed cut-off as per Engineer's requirements



Plan view of the proposed cut-off columns





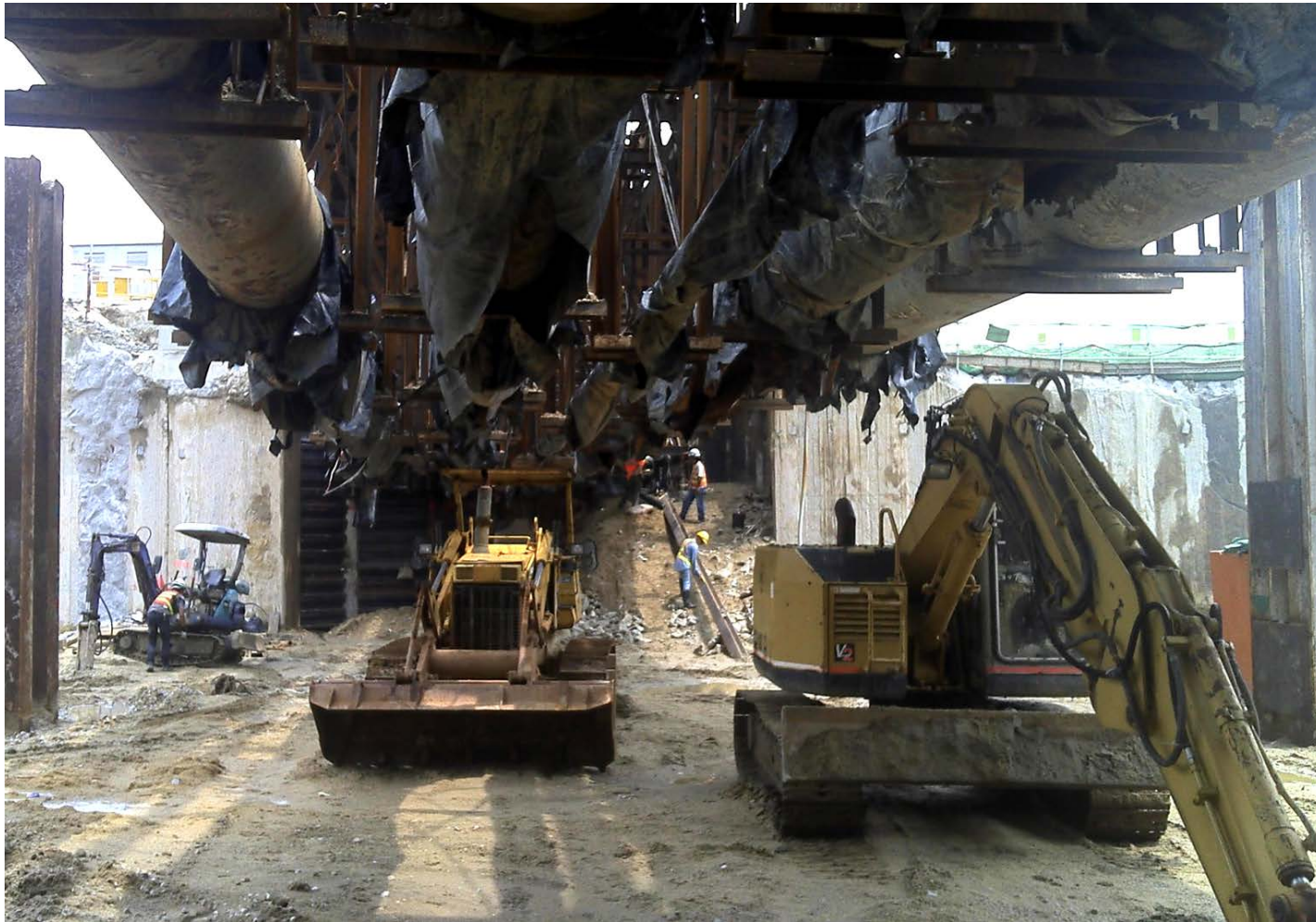
**Preliminary full-scale trial field**





**Whole area kept dry by cut-off columns to enable excavation to proceed**





**Whole area kept dry by cut-off JG columns to enable excavation to proceed**





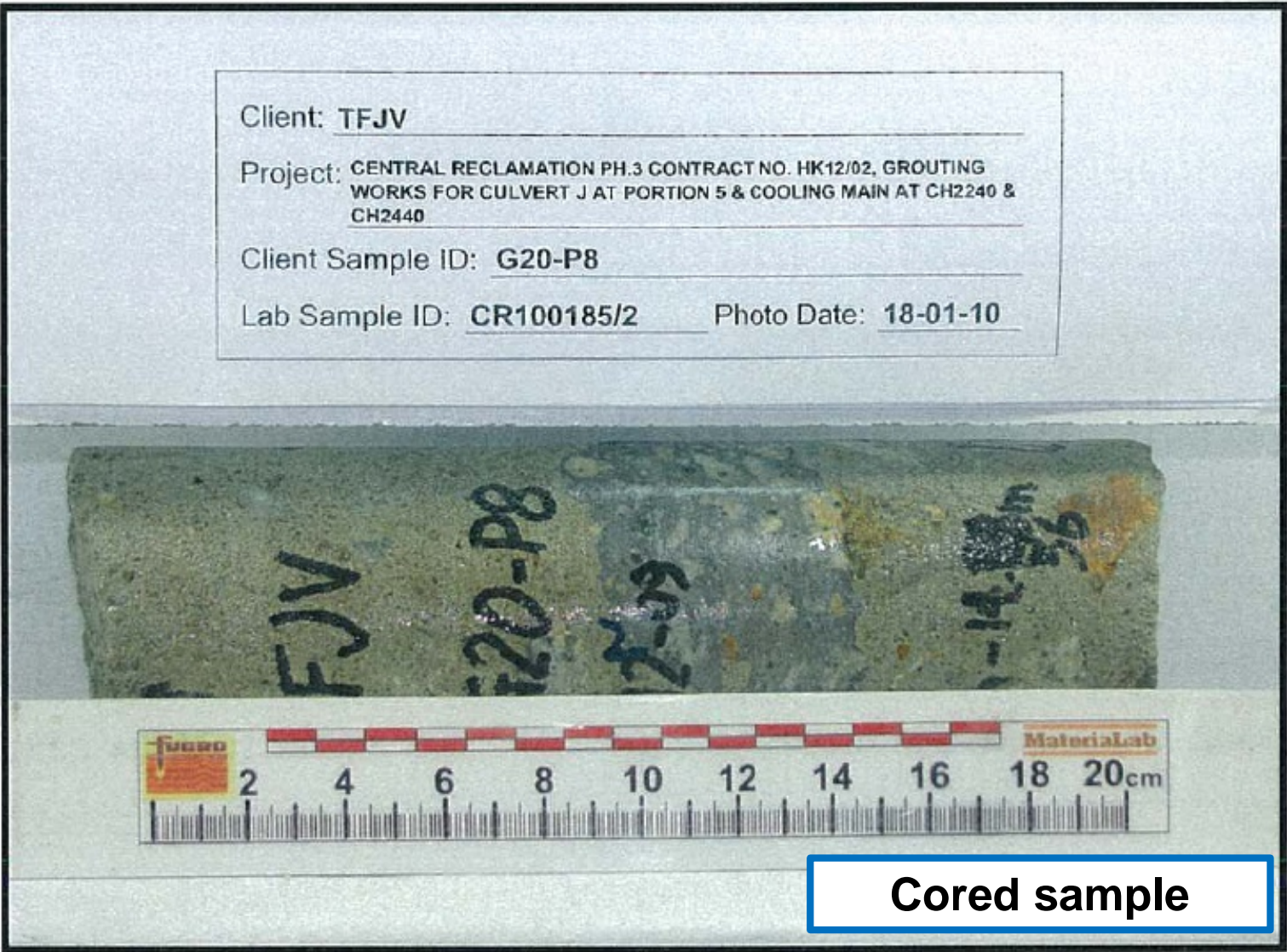
**JG columns formed between vertical piles and cooling mains**





**2.1 m dia. JG columns  
formed between  
vertical piles**

**Excavation in progress**



Cored sample



Test Result

<p>Date Received : 13/01/2010 Date Tested : 22/01/2010 Age of Test : 45 days Condition as Received : Normal</p>	<p><u>Description of Aggregate</u></p> <p>Maximum Size : &lt;5 mm Particle Shape : ANGULAR</p>
<p><u>Compaction of Concrete</u></p> <p>Distribution of Materials : GOOD Presence of Crack : NO Classification of Voids - Small Voids : Few Medium Voids : Few Large Voids : Few (no. of void = 0)</p>	<p>Reinforcement Size(mm) : -- -- -- -- -- Position (mm) : -- -- -- -- -- Spacing(mm) : -- -- -- -- -- Saturated Density : 2120 kg/m³ (without reinforcement)  (volume by water displacement)</p>
<p>Length as Received : Min 215 mm Max 255 mm Length Before Capping : 91.4 mm Length After Capping : 94.0 mm Capping Material : SULPHUR COMPOUND Location from Start of Drilling : 90-185 mm Average Diameter : 83.1 mm Length (after end preparation) / Diameter Ratio : 1.10</p>	<p>Max Load at Failure : 60.3 kN Compressive Strength : 11.0 N/mm² Estimated In-situ Cube Strength : 10.5 N/mm²  Type of Fracture : NORMAL</p>

Test Method : CS1 : 1990 : Section 15 (AMD 1201, 1203 & 1205)

Remarks : \* Sample details supplied by client

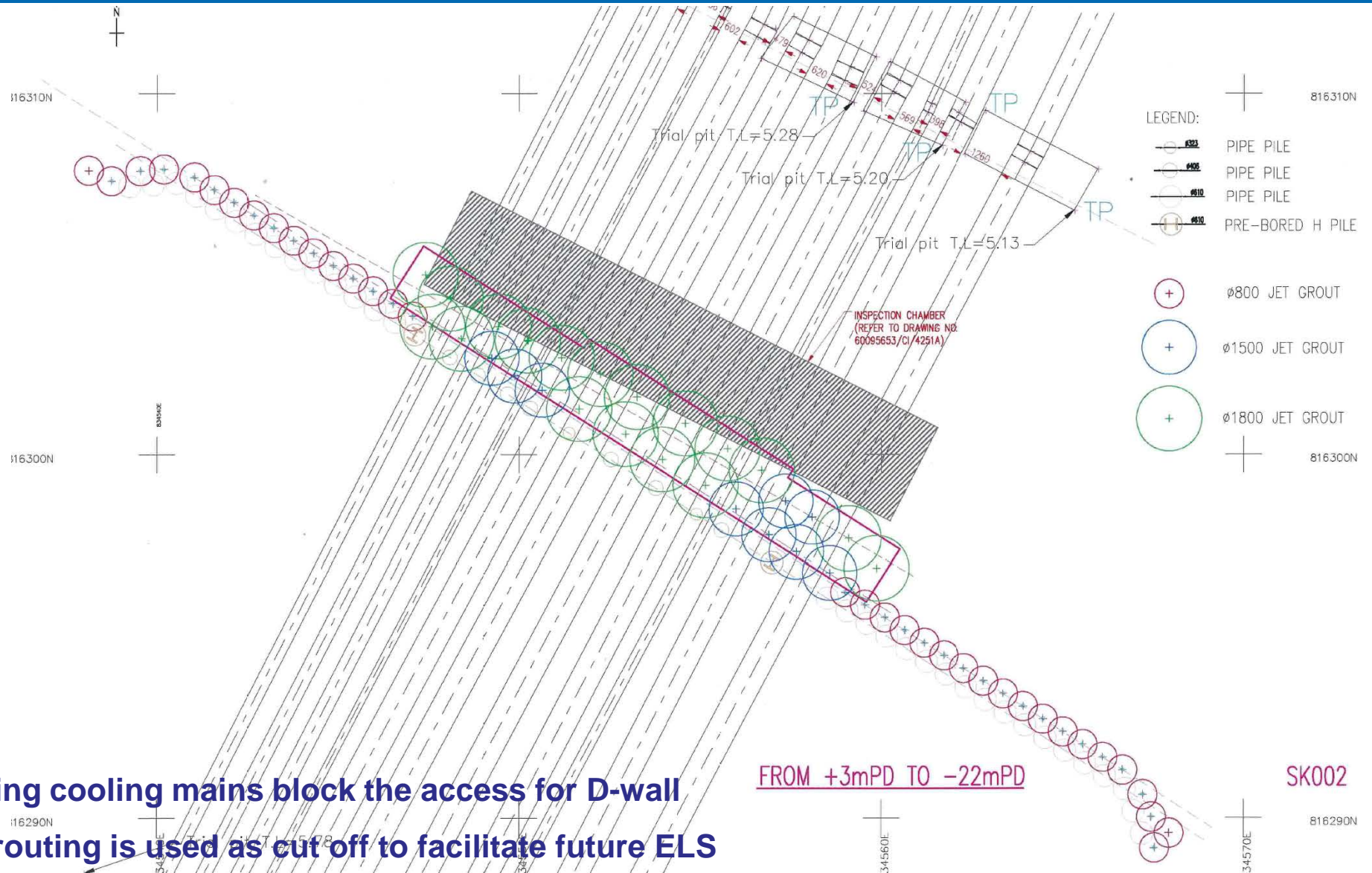
UCS laboratory test  
on cored sample

Test Results

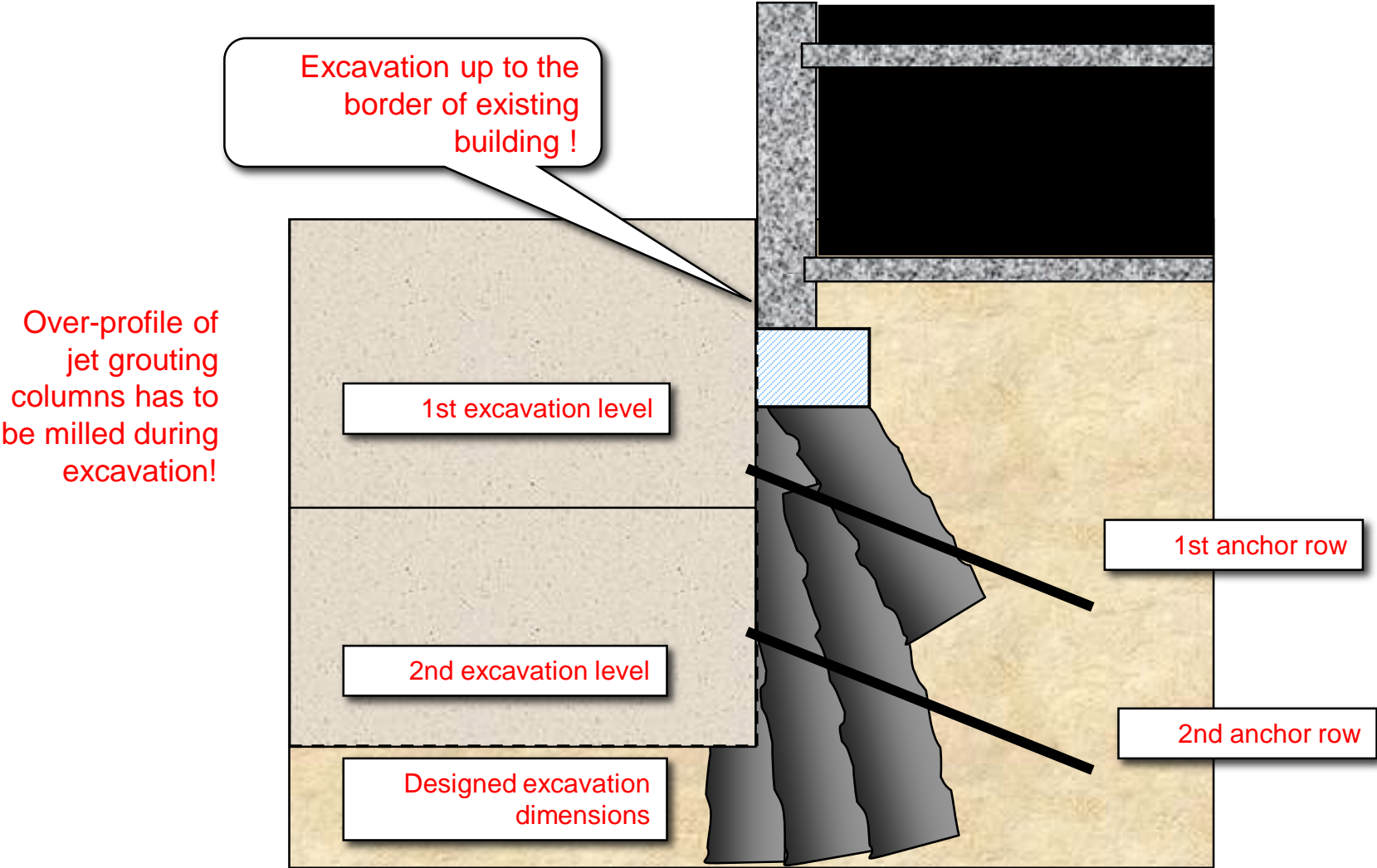
Lab. Sample I.D.	Pipet Reading (ml)		Elapsed Time T (sec.)	Permeation Q (m³)	Coefficient of Permeability K (m/s)
	Start	End			
CN90479/1	3.10	1.15	600	$3.25 \times 10^{-9}$	$1.148 \times 10^{-8}$
	3.10	1.10	600	$3.33 \times 10^{-9}$	$1.118 \times 10^{-8}$
	3.10	1.05	600	$3.42 \times 10^{-9}$	$1.207 \times 10^{-8}$
	3.10	1.10	600	$3.33 \times 10^{-9}$	$1.178 \times 10^{-8}$
	3.10	1.10	600	$3.33 \times 10^{-9}$	$1.178 \times 10^{-8}$
				Average	$1.178 \times 10^{-8}$

Permeability laboratory test on cored sample





- Existing cooling mains block the access for D-wall
- Jet grouting is used as cut off to facilitate future ELS





***Project:*** MTR 1109 – Stations and Tunnels of Kowloon City Section

***Main Contractor:*** Samsung – Hsin Chong JV

***Scope of Works:*** Jet Grouting as soil improvement to avoid settlements on the existing building and structures adjacent the road

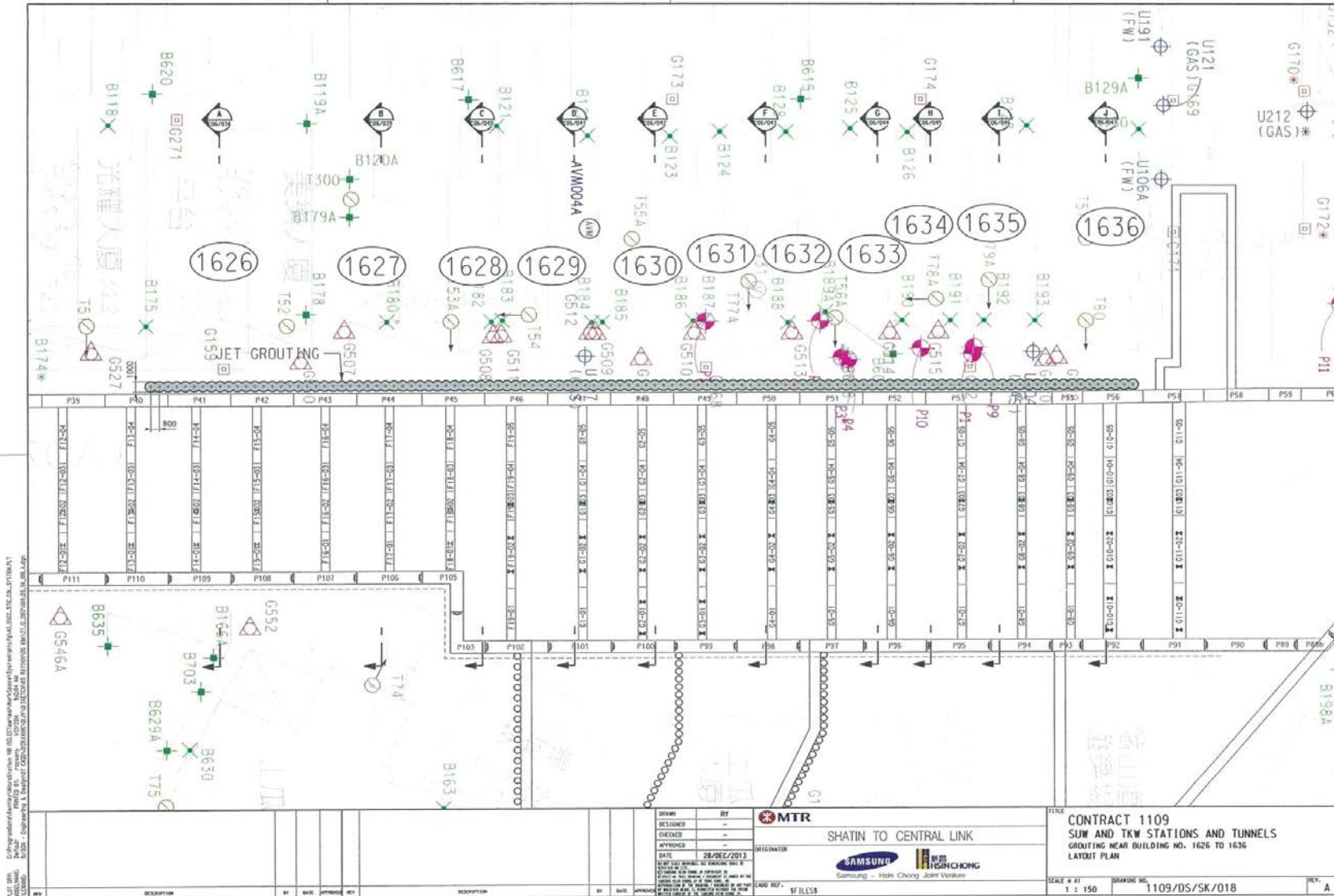
***Progress:*** Job started in December 2013 and was completed in May 2014

## Introduction

- Samsung His Chong JV had been awarded a contract for the construction of MTR stations and tunnels of the Kowloon City Section of the Shatin to Central Link line.
- Part of the tunnel are below To Kwa Wan Road and a diaphragm wall was installed to prevent settlement of the building along the road.
- Jet Grouting was used to: stop the settlements measured during construction of the diaphragm wall and to prevent any settlement during the removal of old piles below the highway.



FILE CONTRACT 1109  
SUW AND TKW STATIONS AND TUNNELS  
GROUTING NEAR BUILDING NO. 1626 TO 1636  
LAYOUT PLAN

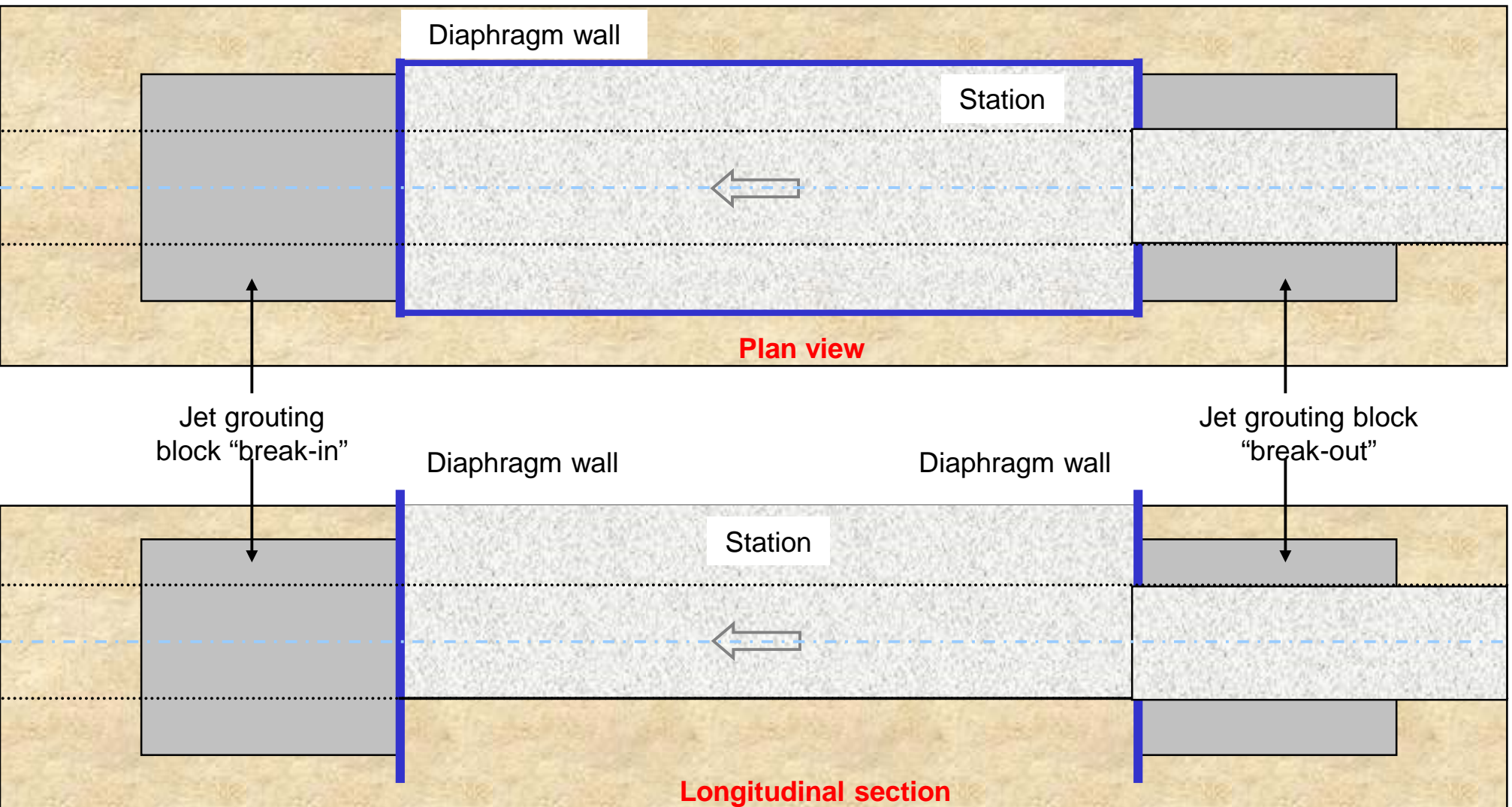








## TBM break-in and break-out







***Project: Lai Chi Kok Drainage Tunnel***

***Consultant: AECOM***

***Main Contractor: Leighton-John Holland JV***

***Scope of Works: Jet Grouting as soil improvement at tunnel break-out***

***Progress: Job started in October 2010 and was completed in March 2011***

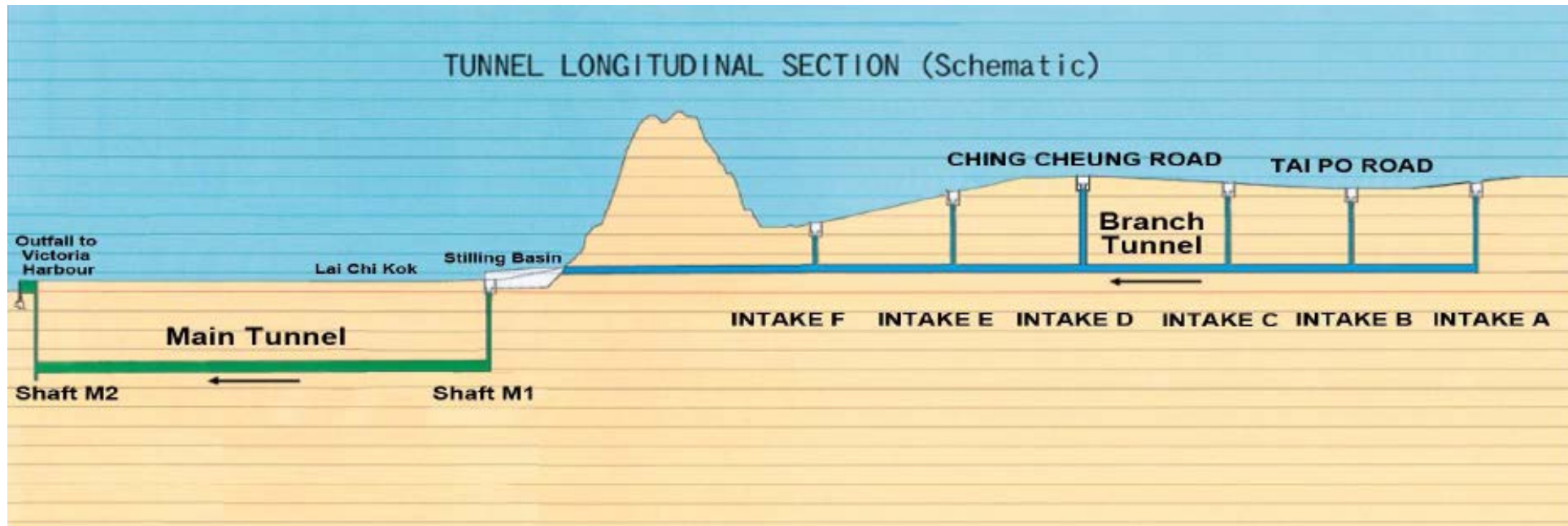
## Introduction

- Leighton John Holland JV had been awarded a contract to construct the Lai Chi Kok Drainage Tunnel
- The tunnel outfall will be at the shaft M2
- The tunnel will be constructed by TBM and break out at M2 whereas site investigation shows that the soil at M2 is of not adequate strength and high permeability.
- Horizontal pressure was designed by the LJHJV as the improvement scheme but TFJV considered jet grouting being a more effective scheme and was awarded the sub-contract based on jet grouting method.



Site General Layout

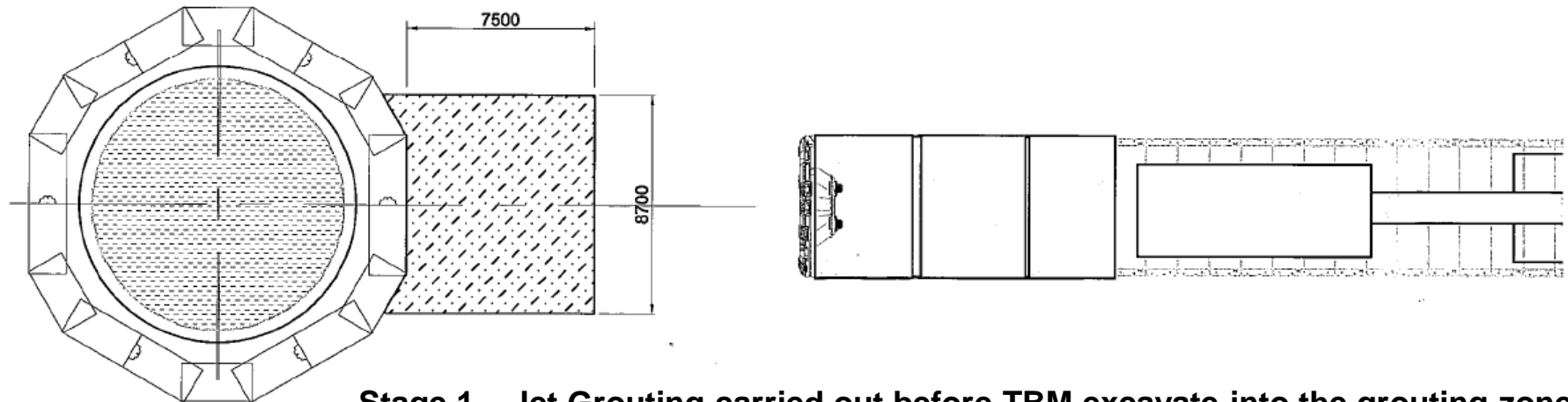




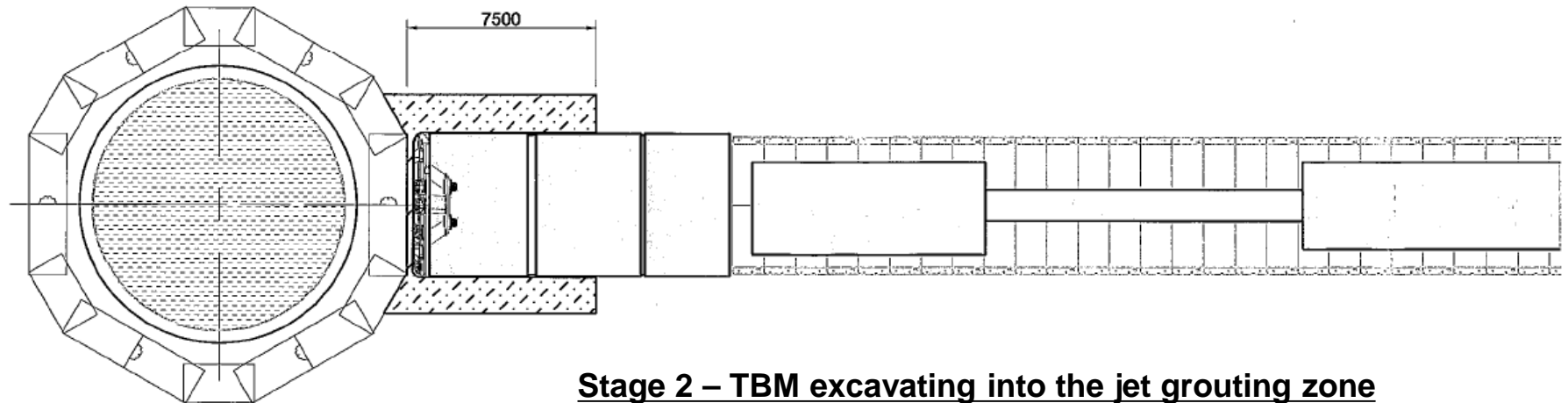
Tunnel Longitudinal Profile



Location of Outfall at Shaft M2



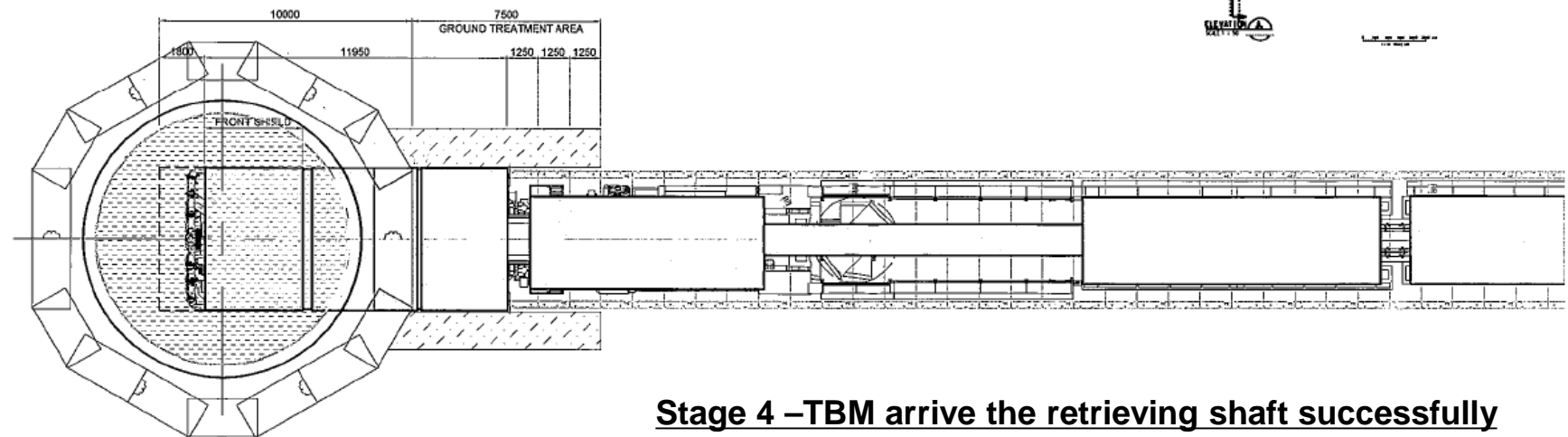
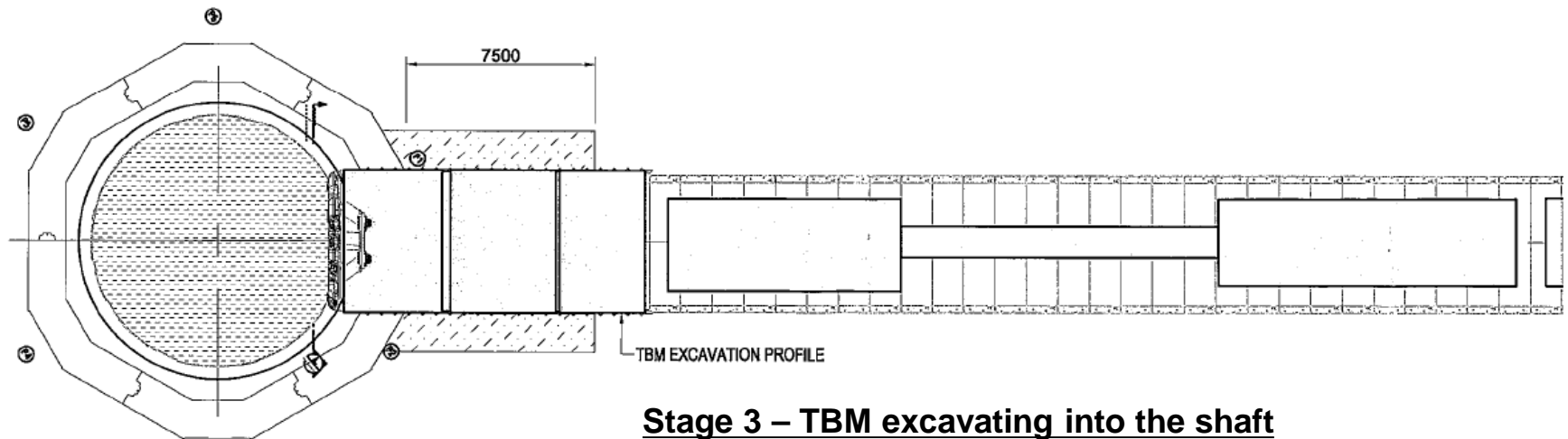
**Stage 1 – Jet Grouting carried out before TBM excavate into the grouting zone**



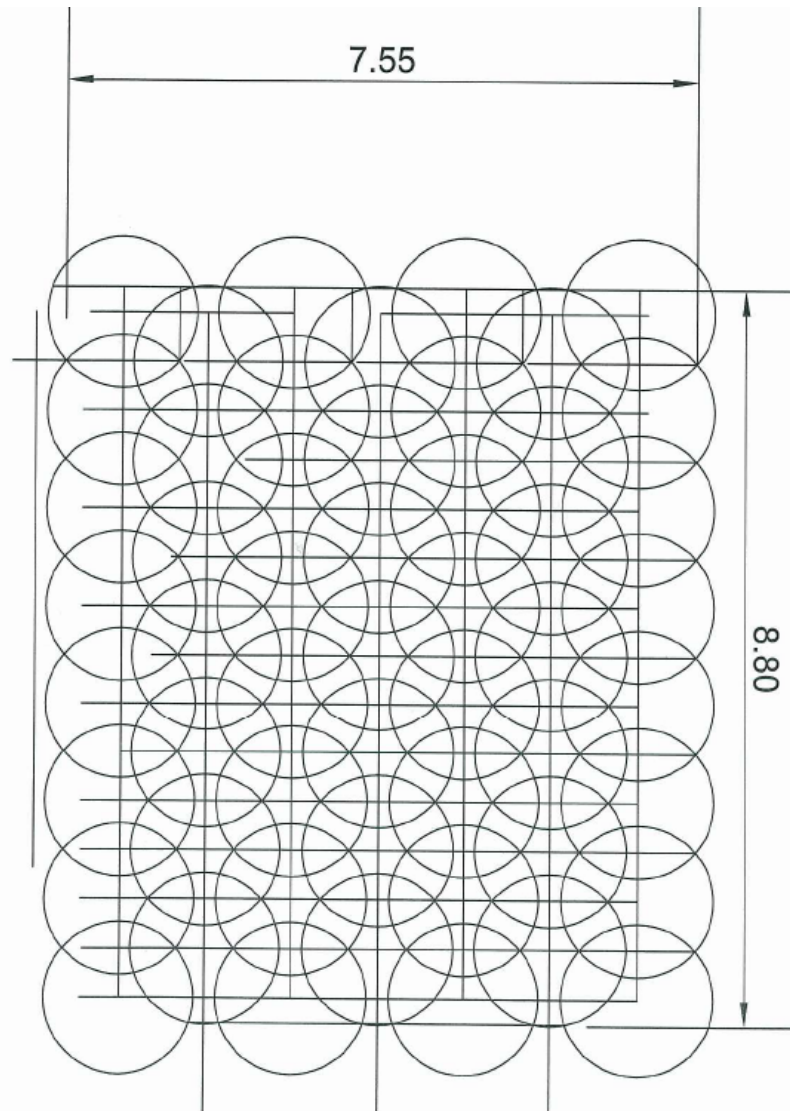
**Stage 2 – TBM excavating into the jet grouting zone**

**Requirement for Jet Grouting work at tunnel breakout (1 of 2)**

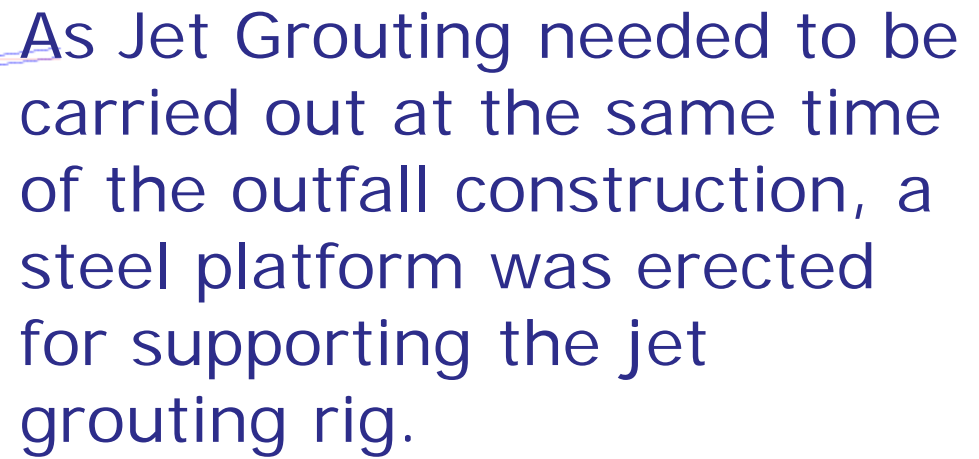




**Requirement for Jet Grouting work at tunnel breakout (2 of 2)**



Proposed 1.8 m diameter jet grouting columns with the spacing shown on the sketch to cover the required treatment area.







**Steel platform erected for supporting the jet grouting rig**



**In-situ permeability test**



**VIBRO**

**FALLING HEAD PERMEABILITY TEST  
RECORD SHEET**

Contractor : VIBRO (H.K.) LIMITED

Contract No. : J201114e

Works Order No. : N/A

Drillhole No. : CH03

Date of Test : 16/03/2011

Ground Level : + 5.60 mPD

Project : 3 Coring Works at Grount Column at Lai Chi Kok

Test No. : 1-1

Co-ordinates :  
E N

Initial Water Level Before Test : 5.88 m below G. L.

Depth of Test : 38.78m to 40.28m

Tested / Supervised By : C. H. Yeung

Checked By : E. Leung

Time Elapsed, t (minutes)	Depth of Water from top of pipe d <sub>t</sub> (m)	ht = d <sub>t</sub> - d <sub>0</sub> (m)	ht / h <sub>0</sub> (h <sub>0</sub> = d <sub>0</sub> - d <sub>0</sub> )
0	0.00	7.55	1.00
0.25	0.03	7.52	1.00
0.5	0.05	7.50	0.99
0.75	0.10	7.45	0.99
1	0.12	7.43	0.98
1.5	0.16	7.39	0.98
2	0.20	7.35	0.97
3	0.24	7.31	0.97
4	0.31	7.24	0.96
5	0.39	7.16	0.95
6	0.44	7.11	0.94
7	0.51	7.04	0.93
8	0.58	6.97	0.92
9	0.64	6.91	0.92
10	0.67	6.88	0.91
15	0.86	6.69	0.87
20	1.22	6.33	0.84
25	1.45	6.10	0.81
30	1.69	5.86	0.78
45	2.28	5.29	0.70
60	2.88	4.67	0.62
90	3.73	3.82	0.51
120	4.36	3.19	0.42
150	4.80	2.75	0.36
180	5.15	2.40	0.32

Note : T is time where ht / h<sub>0</sub> = 0.37  
T = 8760 sec

Permeability  $k = \frac{A}{FT}$   
 $k = 4.10 \times 10^{-8}$  m/sec

d = 0.038 m  
D = 0.101 m  
L = 1.50 m  
hp = 1.67 m  
di = 7.55 m

Where :  
Area =  $A = \frac{\pi d^2}{4} = 0.0011341$  (in metre<sup>2</sup>)  
Intake Factor = F (in metres)  
 $F = \frac{2.4 \pi L}{\ln \left[ \frac{1.2L}{D} + \sqrt{1 + \left( \frac{1.2L}{D} \right)^2} \right]} = 3.16$

Material Surrounding Response Zone :  
Filter Material : Sand Filter

Permeability test results





**Cored samples**

## Maintenance Chamber



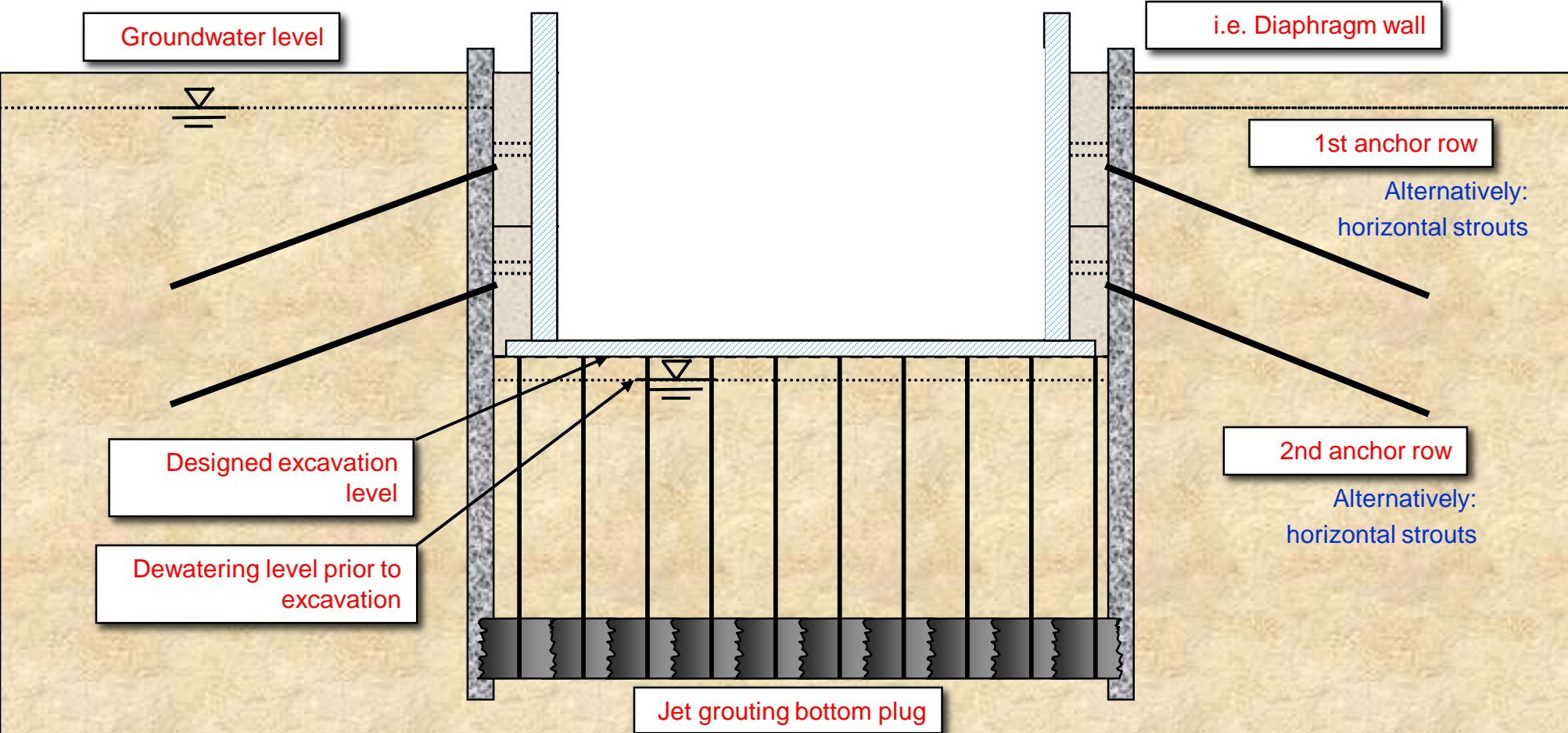
**Views from inside the TBM's head**





**SCL 1107 – Diamond Hill to Kai Tak Tunnels**





Cross section through a typical excavation pit

***Project:*** HKZMB – Hong Kong Boundary Crossing Facilities – Passenger Crossing Building

***Consultant:*** Golder Associates.

***Main Contractor:*** Leighton–Chun Wo JV.

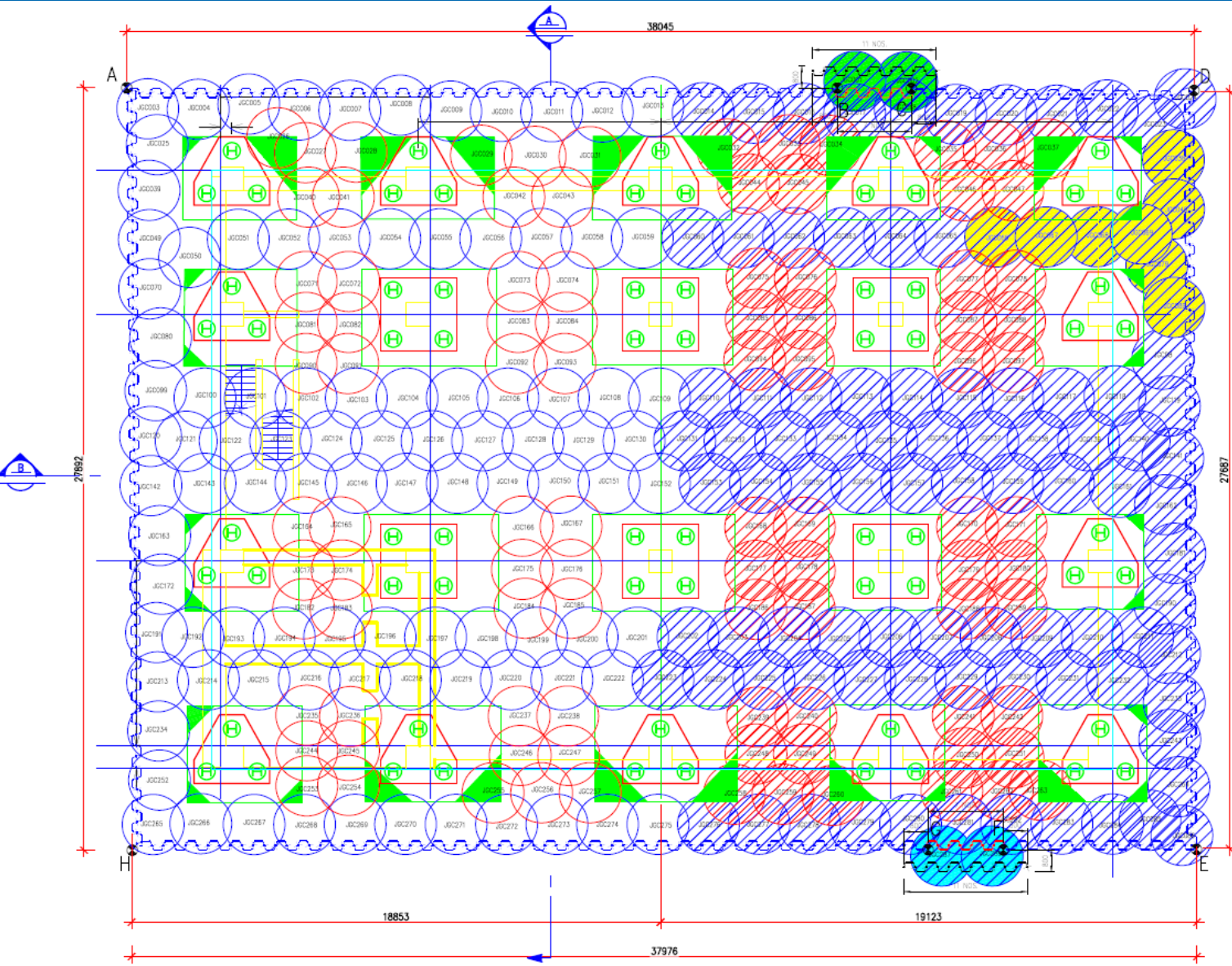
***Scope of Works:*** Jet Grouting as horizontal bottom plug for the seawater pump house.






***Progress:*** Job started in June 2016 and was completed in September 2016.

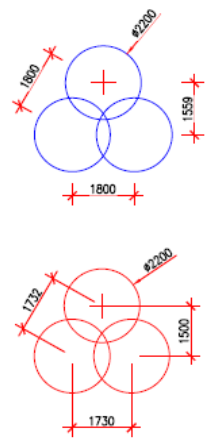
## Introduction

- Leighton-Chun Wo JV had been awarded a contract to construct the Passenger Clearance Building for the Hong Kong–Zhuhai–Macau Bridge – HK Boundary Crossing Facilities.
- Use of Jet Grouting was deemed the best solution to provide a watertight bottom slab below the seawater pumphouse.

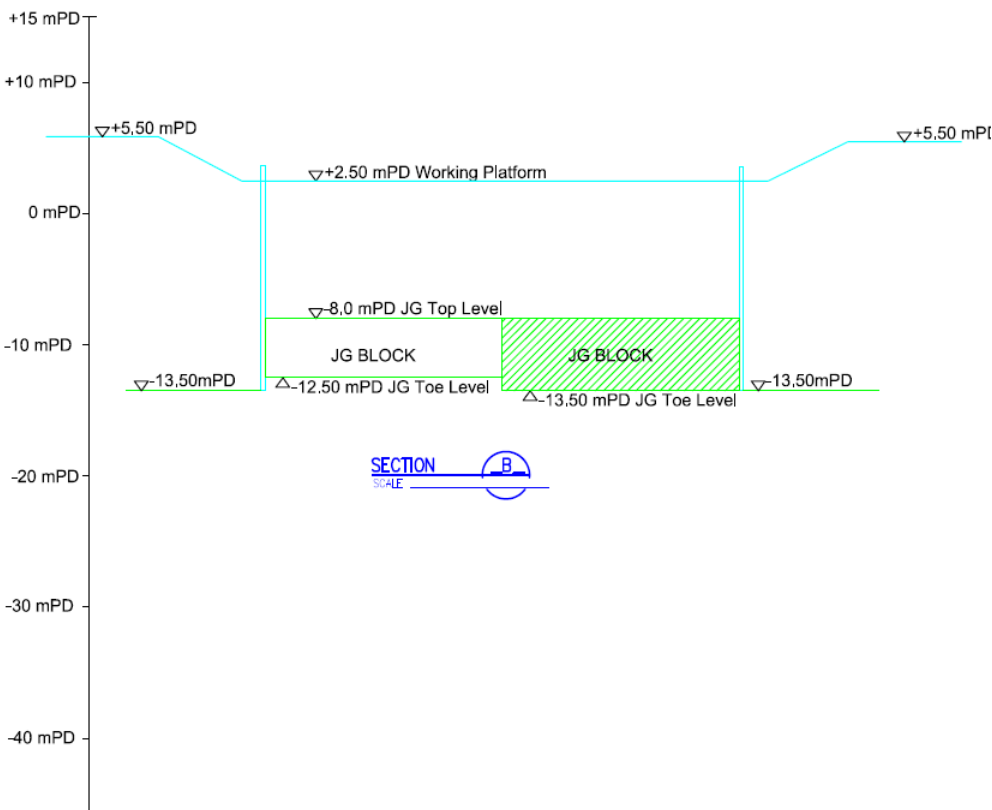
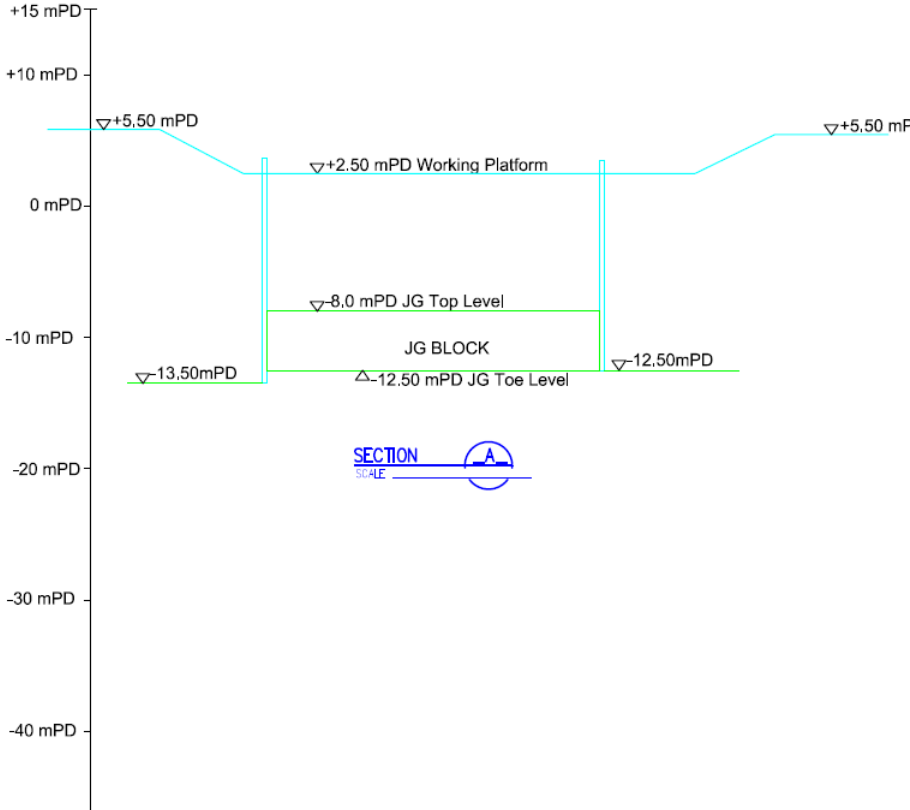




- NOTE:**
-  Cut-Off Level of columns = -6.0 mPD (8 Nos.) (Toe Level = -13.50 mPD)
  -  Cut-Off Level of columns = +2.50 mPD (2 Nos.) (Toe Level = -12.50 mPD)
  -  Cut-Off Level of columns = +2.50 mPD (2 Nos.) (Toe Level = -13.50 mPD)
  -  Cut-Off Level of columns = -8.0 mPD (134 Nos.) (Toe Level = -13.50 mPD)
  -  Cut-Off Level of columns = -8.0PD (142 Nos.) (Toe Level = -12.50 mPD)



TOTAL NO. OF JG COLUMNS = 288

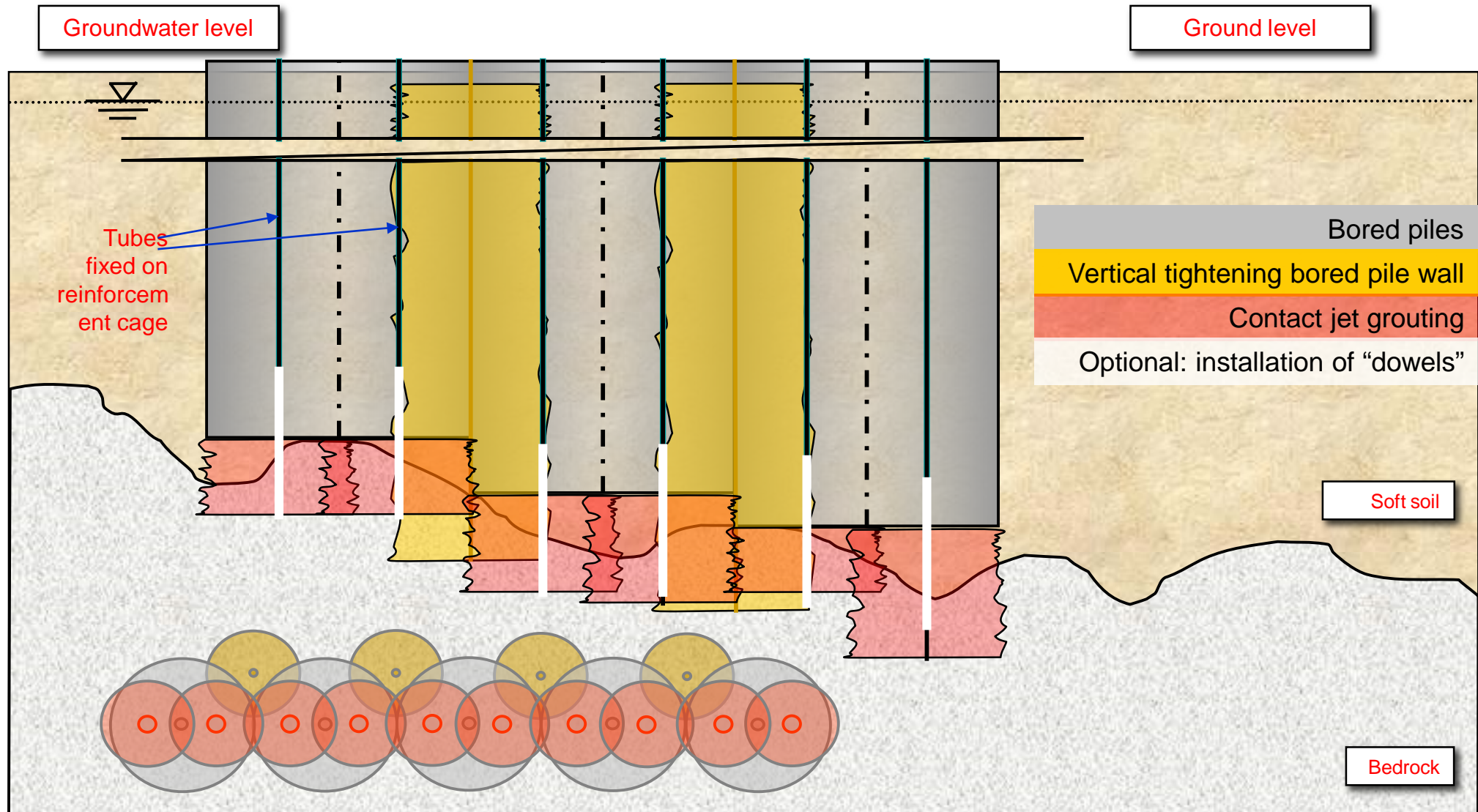








# Watertight contact between piles and bedrock







***Project:** HKZMB – HK Link Road – Section between Scenic Hill and HK Boundary Crossing Facilities*

***Consultant:** ARUP*

***Main Contractor:** CSCEC*

***Scope of Works:** Jet Grouting as watertight contact to rock*

***Progress:** Job started in July 2016 and was completed in August 2016*

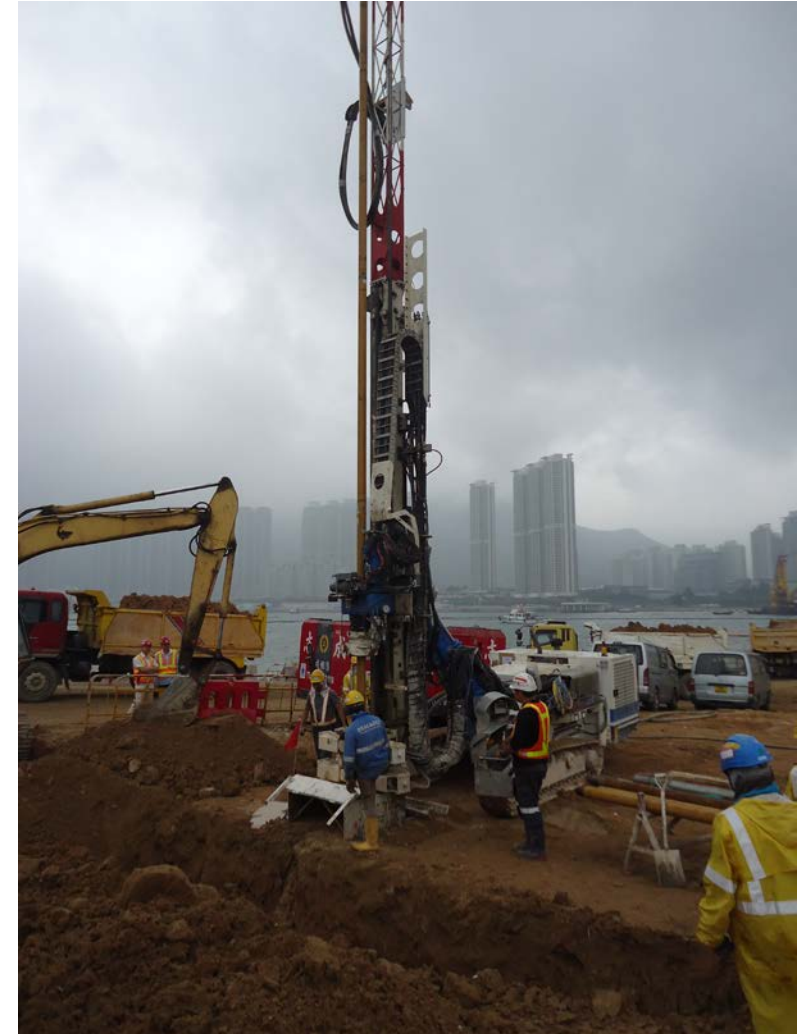


## Introduction

- China State Construction Engineering had been awarded a contract for the construction of the Section between Scenic Hill and HK Boundary Crossing Facilities of the HKZHMB.
- Jet Grouting was proposed and accepted to be used as watertight contact between the pile's toe and the bedrock.









## MTR 810A – West Kowloon Terminus Station North



*Project:* MTR 810A – West Kowloon Terminus Station North

*Main Contractor:* Leighton-Gammon JV

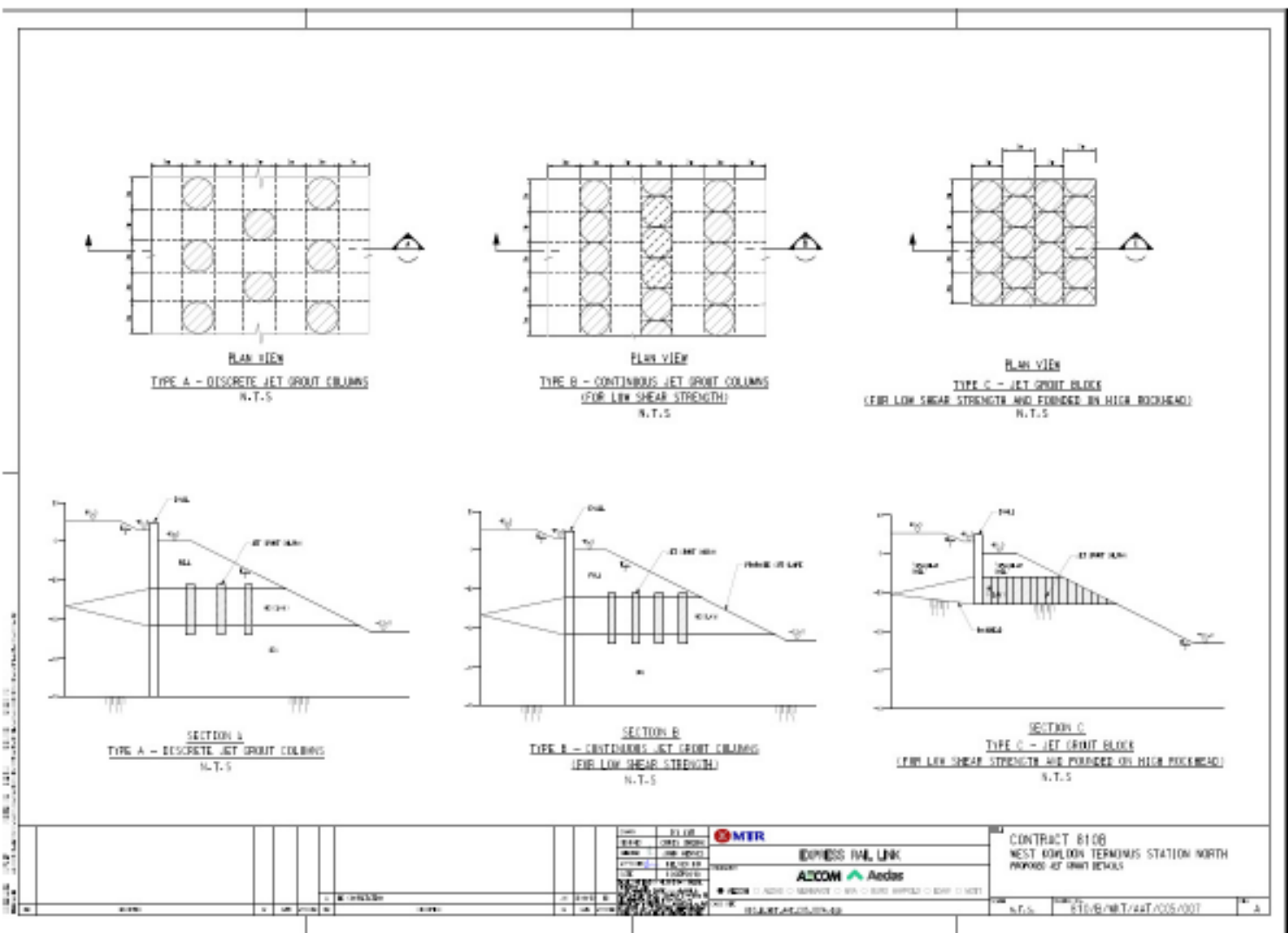
*Consultant:* Arup

*Scope of Works:* Jet Grouting columns to stabilize a slope

*Progress:* Job started in November 2011 and was completed in December 2012































***Project:*** HKZMB – HK Boundary Crossing Facilities – Reclamation Works

***Main Contractor:*** China Harbour Engineering Company Ltd.

***Scope of Works:*** Jet Grouting to consolidate soft and loose soils under an artificial island

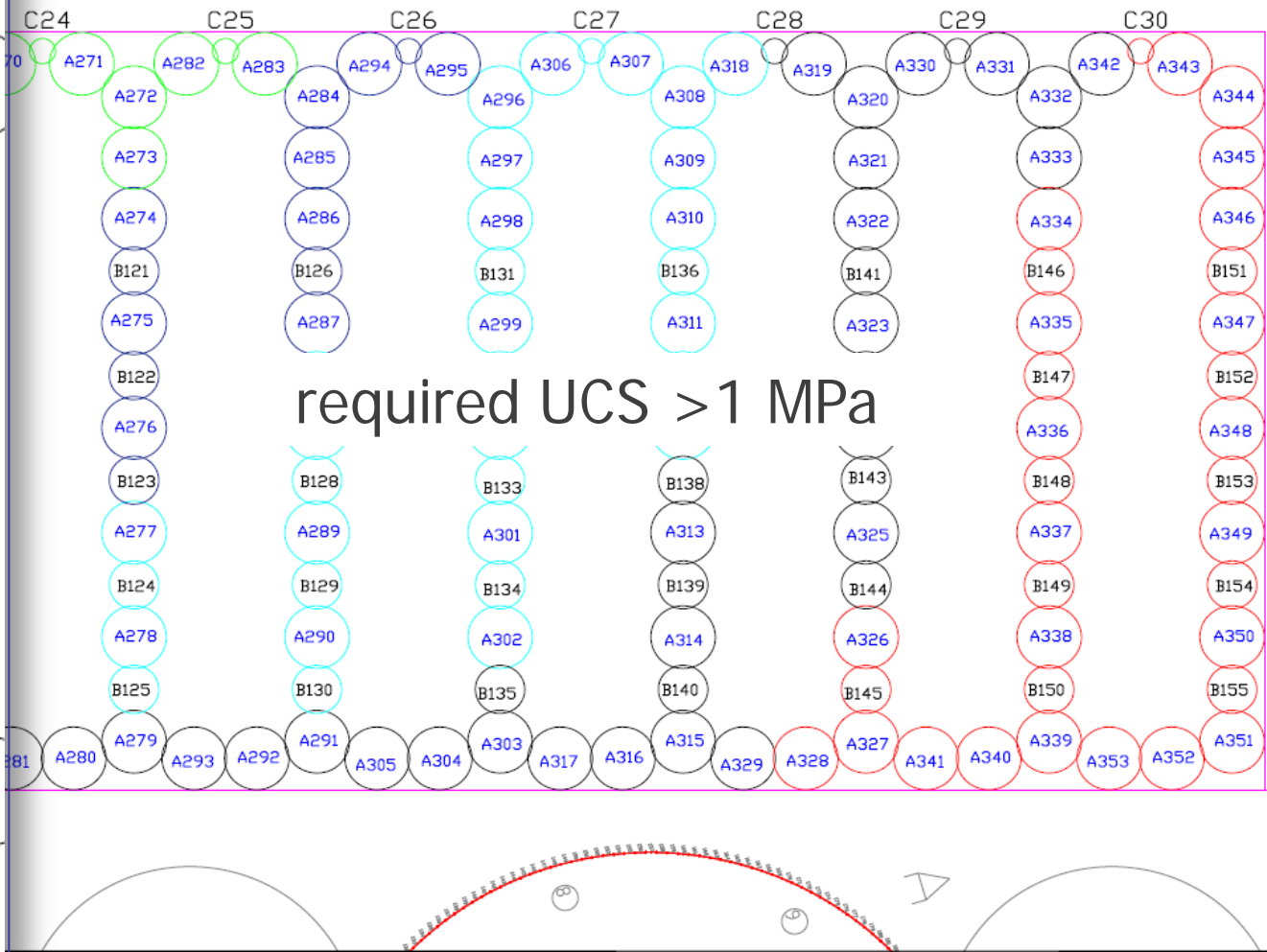
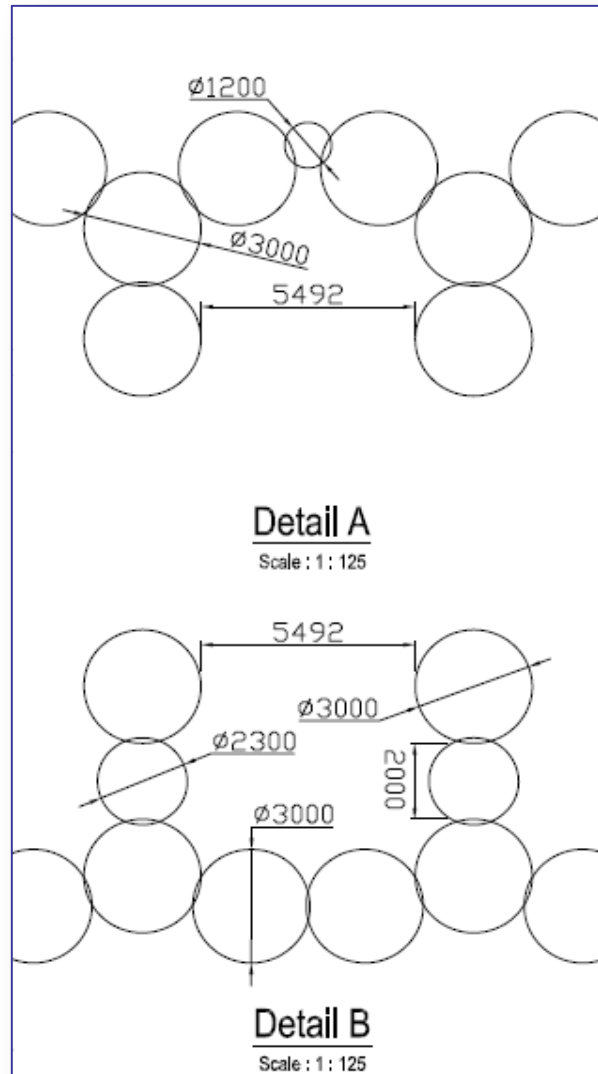
***Progress:*** Job started in March 2015 and was completed in June 2015



## Introduction

- China Harbour Engineering Company Ltd. had been awarded a contract for the reclamation works for the HKZMB – HK Boundary Crossing Facilities.
- Jet Grouting has been adopted to consolidate soft and loose soils below the newly created island.







Grout production batching plant capacity  
up to 1200 cum/day



## 6 Nos. Jetting Rigs Soilmec SM-20





















***QUESTIONS ?***